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## Abstract

The ecological interaction between bacteria and sinking particles, such as bacterial degradation of marine snow particles, is regulated by their encounters. Current encounter models focus on the diffusive regime, valid for particles larger than the bacterial run length, yet the majority of marine snow particles are small, and the encounter process is then ballistic. Here, we analytically and numerically quantify the encounter rate between sinking particles and non-motile or motile micro-organisms in the ballistic regime, explicitly accounting for the hydrodynamic shear created by the particle and its coupling with micro-organism shape. We complement results with selected experiments on non-motile diatoms. The shape-shear coupling has a considerable effect on the encounter rate and encounter location through the mechanisms of hydrodynamic focusing and screening, whereby elongated micro-organisms preferentially orient normally to the particle surface downstream of the particle (focusing) and tangentially to the surface upstream of the particle (screening). Non-motile elongated micro-organisms are screened from sinking particles because shear aligns them tangentially to the particle surface, which reduces the encounter rate by a factor proportional to the square of the micro-organism aspect ratio. For motile elongated micro-organisms, hydrodynamic focusing increases the encounter rate when particle sinking speed is similar to micro-organism swimming speed, whereas for very quickly sinking particles hydrodynamic screening can reduce the encounter rate below that of non-motile micro-organisms. For natural ocean conditions, we connect the ballistic and diffusive limits and compute the encounter rate as a function of shape, motility and particle characteristics. Our results indicate that shear should be taken into account to predict the interactions between bacteria and sinking particles responsible for the large carbon flux in the ocean's biological pump.

## 1. Introduction

Encounters involving small particles suspended in a fluid underpin many industrial, physical and biological processes. In papermaking, too high a collision rate between cellulose fibers leads to excessive fiber flocculation and poor paper quality [1]. In the atmosphere, precipitation formation relies on encounters between water droplets in clouds under the combined action of gravity and turbulence [2]. In the ocean, encounter rates between microscopic phytoplankton following a phytoplankton bloom determine the formation of marine snow responsible for the biological pump, the vertical flux of carbon from the upper ocean to its depths [3]. Living organisms extend the complexity of the encounter processes occurring in non-motile systems by additional mechanisms. Micro-organisms and plankton dwelling in the oceans can navigate through water in search of food and motility greatly enhances the encounter rates of these microscopic organisms with resource patches [4]. Compared to non-motile micro-organisms, whose encounter rate is proportional to the low diffusivity associated with Brownian motion, motile micro-organisms have a much higher (often, 100- to 1000-fold) encounter rate, since their motility effectively enhances diffusivity [4]. Of particular importance for the biogeochemical cycles of carbon in the ocean are the encounters between bacteria and sinking particles of organic matter. Once attached to a particle, bacteria can grow on it and solubilize it, thus reducing the flux of

carbon to the deep ocean [5, 6], a fundamental process in climate-relevant carbon dynamics. Accurate models of the encounter rate between bacteria and particles valid across a wide range of particle sizes are thus important to estimate the role of bacteria in the carbon pump. To date, however, encounter rate formulations have focused on the diffusive regime suitable for large particles. Here, we study the encounter between micro-organisms and sinking particles in the ballistic limit, relevant for the most abundant small particles, with focus on the impact of fluid flow and the associated shear generated by the particle on the encounter rates.

Theoretical estimates of the encounter rates between micro-organisms and sinking particles have thus far primarily built on modeling micro-organisms as spherical colloids and motility as a diffusive process [7, 8]. These simplifying assumptions map the microbial encounter with particles onto the classical problem of heat and mass transfer [8, 9]. By construction, this approach assumes particles are larger than the run length of a bacterium. Since the latter is of the order of tens to hundred of microns [8, 10], the diffusive approximation is limited to particles larger than several hundred microns. Yet, due to the power-law nature of the marine particle size spectrum, the most abundant particles in the ocean have sizes below hundred microns [11]. In this increasingly ballistic regime, the coupling between the flow generated by the particle and the swimming of bacteria may dominate the bacterial orientational dynamics, in contrast to the diffusive regime [12]. There is substantial experimental and theoretical evidence that fluid velocity gradients (shear) can dramatically modify the swimming trajectories of micro-organisms [13–15]. A primary mechanism is shear-induced reorientation, whereby the torque associated with fluid velocity gradients reorients micro-organisms and thus impacts their swimming direction and where they end up in the flow. For example, a simple parabolic flow can lead to shear-trapping and bacterial accumulation near microchannel walls [14]. Shear-induced reorientation is a general phenomenon, applicable to any elongated bacteria that swim in flow, yet its impacts on the fundamental problem of the encounter rate between micro-organisms and sinking aggregates in the ballistic range has to date not been considered.

Here, we combine analytical and numerical calculations with experiments to study encounters between non-motile and motile micro-organisms and sinking particles in the ballistic regime, with focus on how the flow created by the particle affects bacterial trajectories and ultimately the encounter rates. For the classical Stokes flow around a sphere, we show analytically that the orientational dynamics of elongated bacteria—unlike spherical particles—break the fore-aft symmetry of the flow streamlines, with major consequences on encounter rates and attachment location. Non-motile elongated bacteria orient tangentially to the particle surface as they pass by the particle, which reduces their encounter rate by a factor proportional to the square of the bacterial aspect ratio. For motile elongated bacteria, the encounter rate is very sensitive to the particle sinking speed relative to the bacterial swimming speed. When both speeds are comparable, shear increases the encounter rate about twofold and leads to preferential attachment to the leeward side of the particle. For rapidly sinking particles, shear screens motile bacteria from the sinking particle and surprisingly, the encounter rate drops far below the limit corresponding to non-motile bacteria.

This work is organized as follows: we introduce the model of the encounter process and define the relevant observables in section 2. To quantify the impact of shear on bacterial orientation, we classify the asymptotic configurations that ellipsoids assume in general flows and then apply the results to the Stokes flow around a sphere in section 3. The encounter of non-motile and motile micro-organisms with sinking particles is studied in sections 4 and 5. We discuss the biophysical consequences of our mechanistic description of the encounter process in section 6 and draw conclusions in section 7.

## 2. Model

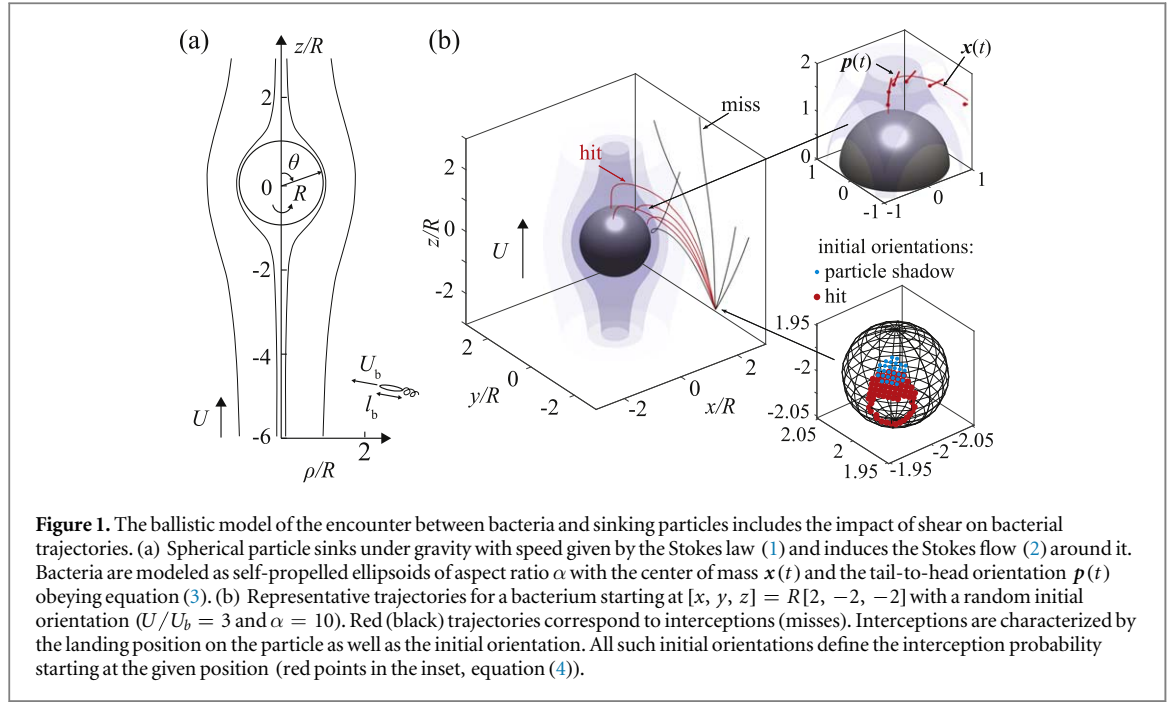
We model a marine snow particle as a sphere sinking in a quiescent fluid and bacteria as elongated and self-propelled ellipsoids (section 2.1). The encounter process is quantified through encounter rate, encounter efficiency and distribution of interception locations (section 2.2).

### 2.1. Equations of motion

The most abundant marine snow particles in the ocean have sizes in the range up to several hundred microns [11] and sinking speeds up to about a millimeter per second [16], which gives Reynolds number up to about 0.1. In this viscosity-dominated regime, the gravitational and viscous forces on the particle balance, implying that a spherical particle of radius  $R$  sinks at the constant terminal speed given by the Stokes law

$$U = \frac{2}{9} \frac{\rho_p / \rho_w - 1}{\nu} g R^2, \quad (1)$$

where  $\rho_p$  and  $\rho_w$  are the densities of the particle and water, respectively,  $\nu$  is the kinematic viscosity of water and  $g$  is the gravitational acceleration. In the reference frame fixed at particle and moving with it (figure 1(a)), the flow



is described by the classic Stokes flow

$$\mathbf{v} = U \cos \theta \left( 1 + \frac{R^3}{2r^3} - \frac{3R}{2r} \right) \hat{\mathbf{r}} - U \sin \theta \left( 1 - \frac{R^3}{4r^3} - \frac{3R}{4r} \right) \hat{\boldsymbol{\theta}}, \quad (2)$$

where  $U$  is the sinking speed given by equation (1).

We model a bacterium as a small self-propelled elongated ellipsoid characterized by three parameters: length  $l_b$ , aspect ratio  $\alpha$  and swimming speed  $U_b$ . The position and orientation of the bacterium at time  $t$  are given by  $\mathbf{x}(t)$  and  $\mathbf{p}(t)$ , where the latter (unit) vector points from the bacterial tail to its head (figure 1(b)). The dynamics of  $\mathbf{x}$  and  $\mathbf{p}$  are governed by

$$\dot{\mathbf{x}} = U_b \mathbf{p} + \mathbf{v}, \quad (3a)$$

$$\dot{\mathbf{p}} = (\mathbf{I} - \mathbf{p}\mathbf{p}^T)(\gamma \mathbf{E} + \mathbf{W})\mathbf{p}. \quad (3b)$$

Equation (3a) states that the total bacterial velocity  $\dot{\mathbf{x}}$  is a superposition of self-propulsion with speed  $U_b$  in the direction  $\mathbf{p}$  and the flow  $\mathbf{v}$  (2) around the particle. Equation (3b) is the classic Jeffery equation for the orientational dynamics of ellipsoids in flow [17]. The tensors  $\mathbf{E}$  and  $\mathbf{W}$  are the symmetric and anti-symmetric parts of the velocity gradient  $A_{ij} = \partial_j v_i$ . The bacterial aspect ratio enters the dynamics (3) through the shape parameter  $\gamma = (\alpha^2 - 1)/(\alpha^2 + 1)$ ; it vanishes for spheres, is positive for elongated organisms and negative for oblate ones. By construction, our model accounts for the hydrodynamic impact of the particle on the bacterium, but neglects the influence of the bacterium on the flow field.

## 2.2. Physical observables

Let  $p(\mathbf{x}, \mathbf{p})$  be the probability of an encounter between the sinking particle and a bacterium starting at the initial position  $\mathbf{x}$  with head pointing in the direction  $\mathbf{p}$ . For the interception criterion, we take the sinking particle to be a perfect absorber and stop simulations if any part of the bacterium touches the particle. For the ballistic model (3),  $p$  is either zero or one since the initial condition  $(\mathbf{x}, \mathbf{p})$  determines a unique bacterial trajectory; when equation (3) is supplemented with rotational diffusion,  $p$  can take a range of values between 0 and 1. Averaging over random orientations yields the encounter probability  $P(\mathbf{x})$  for an initial position  $\mathbf{x}$

$$P(\mathbf{x}) = \int d\mathbf{p} p(\mathbf{x}, \mathbf{p}). \quad (4)$$

Intuitively,  $P(\mathbf{x})$  is the relative solid angle extended by initial bacterial orientations that lead to the interception (red area in the inset of figure 1(b)). Let  $(z, \rho, \phi)$  be the cylindrical coordinate system with origin fixed at the sinking particle. Due to rotational symmetry around the  $z$ -axis, we have  $P(\mathbf{x}) = P(z, \rho)$ . To define the encounter rate and interception efficiency, suppose that the sinking particle enters a region of uniform concentration  $n$  of randomly oriented bacteria. Let  $\hat{N}(t, z)$  be the total number of encounters with bacteria that at time  $t$  are located at a  $z$ -plane below the sinking particle (upstream of the particle,  $z < 0$ ) and collide with the particle at some later time. In a short interval  $(t, t + dt)$ , the change in  $\hat{N}$  due to the encounters with bacteria

with initial positions in the thin sheet ( $z, z + U dt$ ) is  $2\pi n U dt \int_0^\infty P(z, \rho) \rho d\rho$ . Therefore, for a constant sinking speed, the encounter rate  $d\hat{N}/dt(z)$  is independent of time and is given by

$$\frac{d\hat{N}}{dt}(z) = 2\pi n U \int_0^\infty P(z, \rho) \rho d\rho. \quad (5)$$

For a  $z$ -plane far away from the sinking particle  $|z| \gg R$  the fluid is practically undisturbed, making it meaningful to define the  $z$ -independent encounter rate  $\dot{N} = dN/dt$

$$\dot{N} = d\hat{N}/dt(|z| \rightarrow \infty). \quad (6)$$

In simulations, we fix the starting plane at  $z = -6R$ , which amounts to making the approximation  $\dot{N} \approx d\hat{N}/dt(z = -6R)$ . To scale out the concentration  $n$ , we often focus on  $\dot{N}/n$ , the ‘encounter rate kernel’ [8].

To further scale out factors intrinsic to the sinking particle, the radius  $R$  and velocity  $U$ , we follow the notation used in filtration literature and define the dimensionless interception efficiency  $\eta$  as the ratio of volume cleared and volume swept by the particle [9]

$$\eta = \frac{\dot{N}/n}{\pi R^2 U} = \frac{2}{R^2} \int_0^\infty P(\rho) \rho d\rho. \quad (7)$$

Intuitively,  $\eta = 1$  means that the sinking particle collects bacteria from a volume of water equal to the volume of the cylinder the particle sweeps. For small non-motile colloids, we expect  $\eta \ll 1$  because the colloids are constrained to the flow streamlines, which limits the interception to a narrow region near the particle centerline, the ‘stagnation line’ (figure 4(a) and section 4.1).

In addition to computing the encounter rate and encounter efficiency, we will quantify the location on the sinking particle where the bacteria land. Let  $\xi(\theta, \phi)$  be the distribution of the interception locations, where  $\theta$  and  $\phi$  are the colatitude and the azimuth coordinates on the particle, respectively. We normalize  $\xi(\theta, \phi)$  as the probability density function over the unit sphere,  $\int_0^\pi \int_0^{2\pi} \xi(\theta, \phi) d\Omega = 1$ , where  $d\Omega = \sin \theta d\theta d\phi$ . Rotational symmetry implies that  $\xi(\theta, \phi) = \xi(\theta)$ . Finally, the mean interception colatitude is

$$\langle \theta \rangle = \int_0^\pi \int_0^{2\pi} \theta \xi(\theta, \phi) d\Omega = 2\pi \int_0^\pi \theta \xi(\theta) \sin \theta d\theta. \quad (8)$$

For example,  $0^\circ < \langle \theta \rangle < 90^\circ$  (northern hemisphere, downstream) implies preferential leeward attachment, while  $90^\circ < \langle \theta \rangle < 180^\circ$  (southern hemisphere, upstream) indicates attachment to the front.

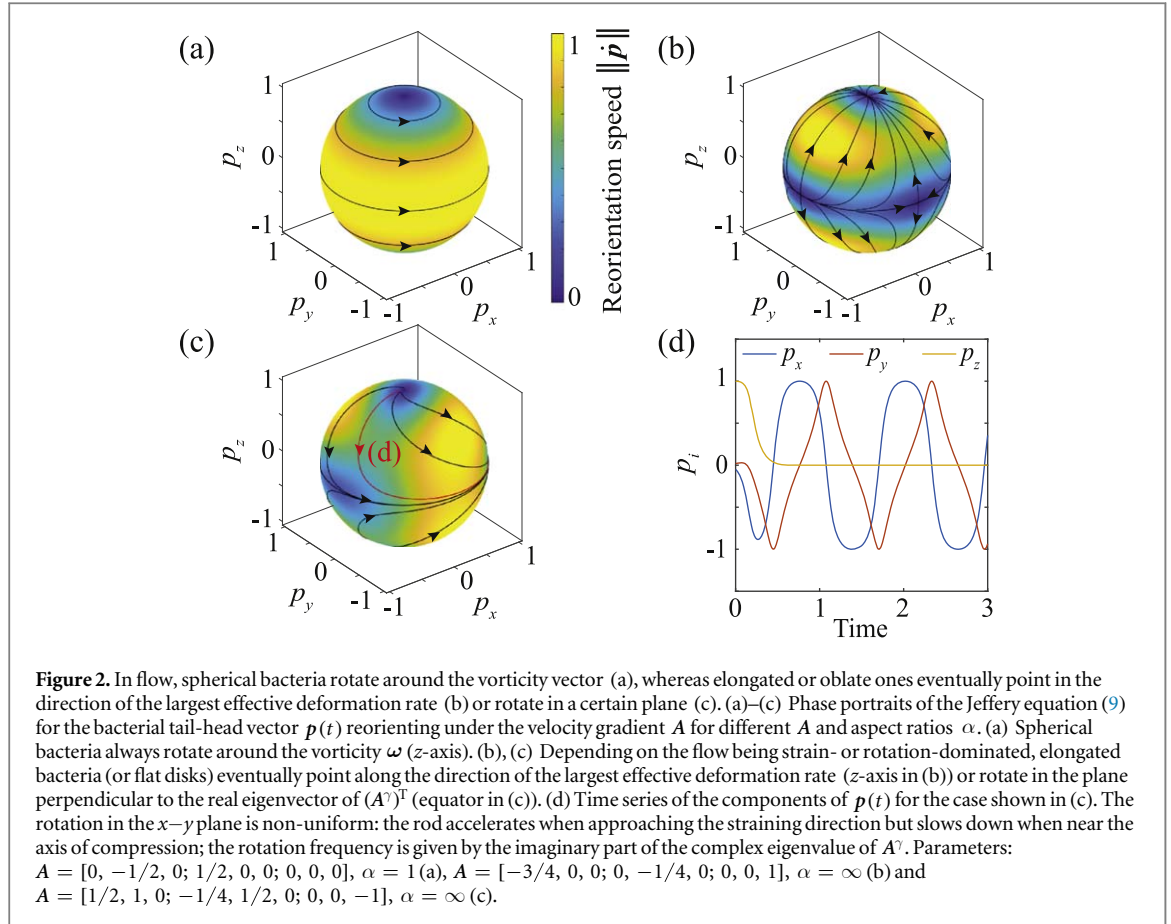
### 3. Ellipsoids in flow

Shear preferentially reorients rods and disks, such as elongated bacteria or flat diatoms, along certain directions. Depending on the flow being strain- or rotation-dominated, ellipsoids eventually point in the direction of the largest deformation rate or rotate in a certain plane (section 3.1). Applying this classification to the Stokes flow induced by the sinking particle reveals that ellipsoids—unlike spheres—break the fore-aft symmetry of the flow streamlines (section 3.2). This quasi-static picture will be essential to rationalize the subsequent simulations of the encounter problem as it underpins the phenomena of hydrodynamic focusing and screening.

#### 3.1. Ellipsoids in general flows

The asymptotic orientation of a non-spherical micro-organism held fixed in flow but free to reorient under the action of the velocity gradient  $A$  follows from the long-time limit of the Jeffery equation (3b). Previous studies focused on special cases with  $A$  derived from, for example, simple shear or rotational flows; in the former case the dynamics collapse onto one of the many degenerate limit cycles, the well-known Jeffery orbits [17, 18]. For a random  $A$ , neglecting marginal cases of  $A$  having eigenvalues with multiplicity greater than one, two scenarios are possible: either a rod asymptotically points towards the direction of the largest effective deformation rate or it rotates in a certain plane. The first possibility has been known [18] and corresponds to the rate of strain  $E$  out-competing the rate of rotation  $W$ . The second scenario complements the study in [19] and generalizes the Jeffery orbits to generic rotational flows and arises when  $W$  dominates over  $E$ . Detailed derivations are given in the appendices A.1 and A.2.

The symmetric part of the gradient  $A$ , the rate of strain  $E$ , describes the rate at which the fluid stretches and compresses [20]. The antisymmetric part  $W$  represents the fluid rate of rotation and is determined by the vorticity  $\omega = \nabla \times \mathbf{v}$  as  $W_{ij} = -\frac{1}{2} \epsilon_{ijk} \omega_k$ . Given  $A$ , it is the weighted sum  $A^\gamma = \gamma E + W$  that enters the Jeffery equation (3b), where  $\gamma$  is the shape parameter  $\gamma = (\alpha^2 - 1)/(\alpha^2 + 1)$  determined by the organism aspect ratio  $\alpha$ . In this notation, the Jeffery equation (9) reads



$$\dot{\mathbf{p}} = (\mathbf{I} - \mathbf{p}\mathbf{p}^\top)\mathbf{A}^\gamma\mathbf{p}. \quad (9)$$

Equation (9) is a dynamical system on the unit sphere of orientations (figure 2). We first discuss the case of spherical micro-organisms ( $\alpha = 1, \gamma = 0$ ) and then describe in detail the response of elongated bacteria ( $\alpha > 1, \gamma > 0$ ); the case of oblate micro-organisms ( $\alpha < 1, \gamma < 0$ ) is dual to that of elongated ones.

For spherical micro-organisms, the shape parameter vanishes ( $\gamma = 0$ ) and equation (9) simplifies to

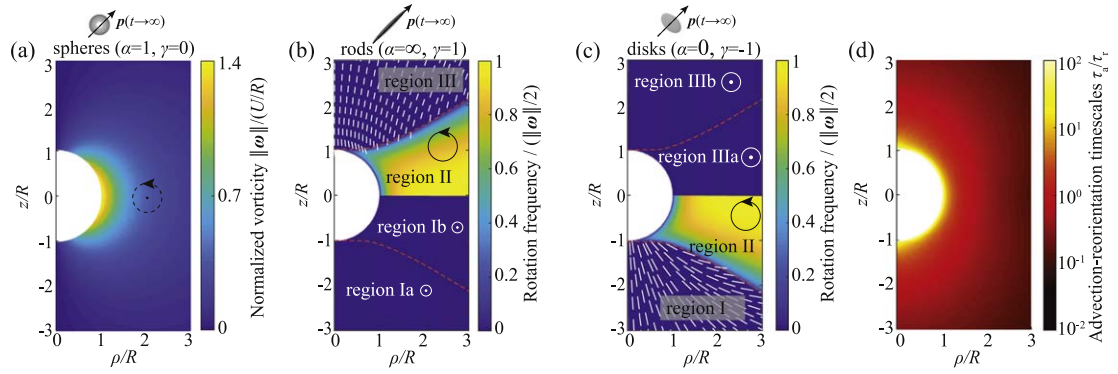
$$\dot{\mathbf{p}} = \frac{1}{2}\boldsymbol{\omega} \times \mathbf{p}, \quad (10)$$

where  $\boldsymbol{\omega}$  is the vorticity. Thus, spherical micro-organisms respond to the fluid rotation but are unaffected by the fluid straining motion. Equation (10) can be solved exactly in this case [18]: for a given initial orientation  $\mathbf{p}(0)$ , the solutions of equation (10) correspond to  $\mathbf{p}(t)$  rotating around the vorticity vector  $\boldsymbol{\omega}$  and in the same sense as  $\boldsymbol{\omega}$  (figure 2(a)). The angle between  $\mathbf{p}(t)$  and  $\boldsymbol{\omega}$  is fixed by the initial orientation and the rotation rate is  $\|\boldsymbol{\omega}\|/2$ .

Elongated or oblate micro-organisms respond to both, the fluid rate of strain and rate of rotation. In this case, it appears impossible to find analytical solutions to equation (9); instead, standard dynamical system theory helps to identify the long-time response. Since the fixed points of equation (9) are given by the real eigenvectors of  $\mathbf{A}^\gamma$  [18], it is the eigendecomposition of  $\mathbf{A}^\gamma$  that determines the asymptotic response. For a random  $\mathbf{A}^\gamma$ , two cases are possible: either  $\mathbf{A}^\gamma$  has three real eigenvalues or one real eigenvalue and two complex conjugate eigenvalues. In the first case, the eigenvector corresponding to the largest positive eigenvalue is an attractive fixed point of (9) (figure 2(b)). In the second case, when the real eigenvalue is positive, the corresponding eigendirection is still attractive, but once this eigenvalue is negative, the eigendirection becomes unstable and the dynamics collapse onto a limit cycle (figure 2(c)). We next discuss these asymptotic scenarios in more detail.

Let  $\lambda_i$  and  $\boldsymbol{\lambda}_i$ , where  $i = 1, 2, 3$ , be the eigenvalues and eigenvectors of  $\mathbf{A}^\gamma$ . The incompressibility of the flow requires that  $\lambda_1 + \lambda_2 + \lambda_3 = 0$ . When all  $\lambda_i$ 's are real, the Jeffery equation (9) has three pairs of fixed points corresponding to  $\mathbf{p} = \pm\boldsymbol{\lambda}_i$ . Assuming that  $\lambda_1 < \lambda_2 < \lambda_3$ , the fixed points are respectively: a repulsive node ( $\boldsymbol{\lambda}_1$ ), a saddle ( $\boldsymbol{\lambda}_2$ ), and an attractive node ( $\boldsymbol{\lambda}_3$ ). As a consequence, a random initial orientation eventually collapses onto the stable direction  $\mathbf{p} = \pm\boldsymbol{\lambda}_3$  (figure 2(b)). The timescale  $\tau_{\lambda_3}$  associated with this reorientation is estimated as inverse of the average of the eigenvalues of the linearized version of equation (9) near the fixed point  $\boldsymbol{\lambda}_3$  and is given by  $\tau_{\lambda_3}^{-1} = \frac{3}{2}\lambda_3$ . Since the system orients along  $\pm\boldsymbol{\lambda}_3$ , the case when all  $\lambda_i$ 's are real corresponds to the rate of strain  $\mathbf{E}$  outcompeting the rate of rotation  $\mathbf{W}$ .





**Figure 3.** Non-spherical micro-organisms break the fore-aft symmetry of the Stokes flow around a sinking particle as revealed by their asymptotic orientation when held fixed in the flow. The velocity gradient  $A$  (equation (13)) determines the local long-time orientation of the bacterial tail-to-head vector  $p(t)$  (figure 2). (a) Spherical bacteria respond symmetrically upstream and downstream of the particle:  $p$  rotates around the vorticity  $\omega \propto \hat{\phi}$  and in the same sense as  $\omega$  (arrow); the broken line indicates that there are many possible orbits (figure 2(a)). (b) Perfect rods exhibit three regions of different asymptotic orientations. In regions I and III the rate of strain outcompetes the vorticity (figure 2(b)), whereas the vorticity dominates in the region II (figure 2(c)). Specifically, in the upstream region I, bacteria eventually point along the azimuth  $p = \pm \hat{\phi}$ . The two subregions inside the region I differ only by how the asymptotic orientation is attained (attractive node versus spiral). In region II,  $p$  eventually rotates in the plane perpendicular to  $\hat{\phi}$  (figure 2(c)). The color code shows the rotation rate normalized by  $\|\omega\|/2$ ; the sense of rotation is the same as  $\omega$  (solid line and arrow). In the downstream region III,  $p$  orients along the director field (white lines) defined by  $\lambda_1$  in equation (15). (c) For perfect disks, the response is a reflection of the case of perfect rods. (d) Ratio between the advective and reorientation timescales,  $\tau_a$  and  $\tau_r$ . For  $\tau_a/\tau_r \gg 1$ , we expect non-motile micro-organisms advected by the flow to follow the quasi-static reorientation effects described in (b), (c); these reorientation effects are strongest near the sinking particle.

When  $A^\gamma$  has a pair of complex eigenvalues  $\lambda_1$  and  $\lambda_1^*$ , and a real eigenvalue  $\lambda_3$ , the eigenvectors corresponding to  $\{\lambda_1, \lambda_1^*\}$  are complex, implying that there are only two fixed points given by  $p = \pm \lambda_3$ . When  $\lambda_3 > 0$  (stretching), the fixed point  $\lambda_3$  is an attractive spiral and represents the asymptotic direction. The appearance of complex eigenvalues signals the rising importance of the rate of rotation  $W$ , but when  $\lambda_3 > 0$ , straining still dominates the response. However, when  $\lambda_3 < 0$  (compression), the fixed point  $\lambda_3$  becomes a repulsive spiral and a stable limit cycle emerges. The timescale  $\tau_{\lambda_3}$  of spiraling onto or away from  $\lambda_3$  is  $\tau_{\lambda_3}^{-1} = \frac{3}{2}|\lambda_3|$ . The limit cycle corresponds to a great circle; the circle lies in the plane with normal direction given by  $\lambda_3'$ , the eigenvector of the transpose matrix  $A^{\gamma T}$  with eigenvalue  $\lambda_3$ . Thus, when  $\lambda_3 < 0$ , the asymptotic state of equation (9) corresponds to  $p$  rotating in the plane normal to  $\lambda_3'$  (figure 2(c)). The angular frequency of the rotation is given by the imaginary part of the complex eigenvalue  $\lambda_1$  (figure 2(d)).

The above analysis applies to a velocity gradient  $A^\gamma$  under the assumption that all its eigenvalues are different; a separate analysis is required in the degenerate case. We next study  $A$  derived from the Stokes flow around a sinking sphere.

### 3.2. Ellipsoids in the Stokes flow

The above classification of the orientational response of a micro-organism is now specified to the velocity gradient derived from the Stokes flow in equation (2). Physically, we describe a bacterium rotating freely under shear but with the center of mass fixed at some position. Self-propulsion and advection are still not included and this simplification makes analytical progress possible. The long-time orientation depends on bacterial position: spherical bacteria respond identically upstream and downstream of the sinking particle (figure 3(a)), whereas non-spherical ones break the streamline fore-aft symmetry (figures 3(b), (c)). This symmetry breaking leads to hydrodynamic focusing and screening, crucial shear-induced mechanisms that impact the full encounter problem.

Spherical bacteria respond solely to the fluid vorticity (section 3.1), which for the Stokes flow reads

$$\omega = -\frac{3}{2}UR \frac{\sin \theta}{r^2} \hat{\phi}. \quad (11)$$

It follows from equation (11) that bacteria rotate around the azimuth  $\hat{\phi}$ , (figure 3(a)). The rotation rate decays with the square of the distance from the particle; it is strongest to the side of the particle, near the equator  $\theta = \pi/2$  and vanishes near the stagnation lines  $\theta = 0$  and  $\theta = \pi$ . In particular, the response of spherical bacteria preserves the fore-aft symmetry of the flow streamlines: at a fixed distance  $r$ , the bacterial rotation is identical at colatitudes  $\theta$  and  $\pi - \theta$ . As discussed next, this symmetry is broken for elongated or oblate micro-organisms.

We focus on perfect rods of infinite aspect ratio  $\alpha \rightarrow \infty$ , for which the shape factor  $\gamma = 1$  in the Jeffery equation (3b) (figure 3(b)). Note that moderate elongation gives  $\gamma$  close to unity: for an aspect ratio  $\alpha = 10$ ,  $\gamma \approx 0.98$ . The analysis of the response of disks is dual to that of rods and we only state the results (figure 3(c)). For perfect rods, the rates of strain and rotation,  $E$  and  $W$ , are weighted equally in the Jeffery equation (9), which reduces to ( $A^{\gamma=1} = A$ )

$$\dot{p} = (I - pp^T)Ap, \quad (12)$$

where  $A$  is the velocity gradient derived from the Stokes flow (2). For brevity, we take  $U = 1$  and  $R = 1$ . In spherical coordinates  $\{r, \theta, \phi\}$  and in the usual basis of unit vectors  $\{\hat{r}, \hat{\theta}, \hat{\phi}\}$ , the entries of  $A$  read (appendix A.3, see also [21])

$$A_{ij} = F(r, \theta) \begin{bmatrix} 2 & \tan \theta & 0 \\ -\beta(r) \tan \theta & -1 & 0 \\ 0 & 0 & -1 \end{bmatrix}, \quad (13)$$

where  $F = 3 \cos \theta (r^{-2} - r^{-4})/4$  and  $\beta = (r^2 + 1)/(r^2 - 1)$ . To classify the response of rods in the manner outlined in section 3.1, we find the eigenvalues of  $A$

$$\lambda_{1,2} = \frac{F}{2} (1 \pm \sqrt{9 - 4\beta \tan^2 \theta}), \quad \lambda_3 = -F, \quad (14)$$

and the corresponding eigenvectors

$$\lambda_{1,2} = [1, \frac{-3 \pm \sqrt{9 + 4\beta \tan^2 \theta}}{2 \tan \theta}, 0], \quad \lambda_3 = \hat{\phi}. \quad (15)$$

From the sign change under the square root in equation (14), it follows that the regions in the fluid in which  $A$  has three real eigenvalues or a pair of complex eigenvalues plus a real eigenvalue are separated by two surfaces of revolution defined by (broken red lines in figures 3(b), (c))

$$r^2(\theta) = (9 + 4 \tan^2 \theta) / (9 - 4 \tan^2 \theta). \quad (16)$$

Furthermore, in the region with complex eigenvalues, the real eigenvalue,  $\lambda_3 = -F(r, \theta)$ , changes sign from negative to positive at the plane  $\theta = \pi/2$ , which contains the sinking particle's equator. Physically, the sign change reflects the transition of  $\lambda_3 = \hat{\phi}$  from being the direction of fluid expansion to compression as the fluid parcels travel from the southern to the northern hemisphere. The surfaces (16) and  $\theta = \pi/2$  divide the space outside the particle into three regions I, II and III (figure 3(b)). Region I is the bottom-half of the entire domain, below the equator plane  $\theta = \pi/2$  and upstream of the sinking particle. It is composed of two subregions, Ia and Ib, separated by the surface (16) (lower broken red line in figure 3(b)). In Ia, all the eigenvalues are real, in Ib, there is a pair of complex eigenvalues and a positive real eigenvalue  $\lambda_3 > 0$ . In both subregions, the rate of strain dominates over the rate of rotation and the asymptotic stable direction is given by the eigenvector  $\lambda_3 = \hat{\phi}$ , which always points along the azimuth. The two subregions differ only in the manner this asymptotic orientation is approached: in Ia, the convergence is overdamped (as in figure 2(b)) since  $\hat{\phi}$  is an attractive node, in Ib, the convergence is underdamped with the bacterium spiraling down onto  $\hat{\phi}$  since this fixed point is an attractive spiral (as in figure 2(c) but with arrows reversed). This change in the nature of the convergence of  $p$  onto  $\hat{\phi}$  indicates the increasing role of vorticity near the particle equator, but  $\hat{\phi}$  remains the attractive fixed point in region I because the fluid has to expand along the azimuth to accommodate the sinking sphere in that region. The timescale  $\tau_I$  associated with convergence onto  $\hat{\phi}$  in region I is  $\tau_I^{-1} = \frac{3}{2}\lambda_3 = -\frac{3}{2}F$ .

Region II lies to the side of the particle, in between the equator plane and the surface (16) and is the only region in which the rotation rate out-competes the rate of strain. In this region,  $\lambda_{1,2}$  are complex and  $\lambda_3 < 0$ ; physically, the fluid is being compressed along the azimuth as it is rolling over the particle surface due to the no-slip boundary conditions. The analysis in section 3.1 implies that the rods eventually rotate in the plane orthogonal to the azimuth with frequency  $F/2\sqrt{4\beta \tan^2 \theta - 9}$ . Thus, rods orient orthogonal to the vorticity  $\omega$  and rotate in the same sense as  $\omega$ , but the rotation period is longer from the rotation rate of the fluid (color code in region II in figure 3(b)). The timescale  $\tau_{II}$  associated with the reorientation from pointing along  $\hat{\phi}$  to rotating in the plane perpendicular to  $\phi$  is given by  $\tau_{II}^{-1} = \frac{3}{2}|\lambda_3| = \frac{3}{2}F$ .

Region III lies downstream of the particle, above the surface (16). Here, the strain once again dominates over rotation, but this time the asymptotic direction of rods in flow is given by the eigenvector  $\lambda_1$  (the white director field lines in figure 3(b)). Importantly, just behind the particle, for small colatitudes  $\theta$ , equation (15) clearly predicts that the stable orientation is approximately the radial direction  $\lambda_1 \approx [1, 0, 0]$ . The timescale  $\tau_{III}$  associated with the reorientation from rotating in the plane perpendicular to  $\phi$  in region II to pointing along  $\lambda_1$  is  $\tau_{III}^{-1} = \frac{3}{2}\lambda_1 = \frac{3}{4}F(1 + \sqrt{9 - 4\beta \tan^2 \theta})$ .

The response of perfect disks ( $\alpha = 0$ ,  $\gamma = -1$ ) is dual to the case of perfect rods since  $A^{\gamma=-1} = -E + W = -A^T$ . For brevity, we only summarize the results, which are essentially an upside-down version of the



responds of rods (figure 3(c)). Upstream of the sinking particle, disks tend to be oriented almost tangentially to the particle, with their symmetry axis pointing in the nearly radial direction (region I, white director lines in figure 3(c)). To the side of the particle, disks rotate, with their axis of symmetry spinning in the  $r$ - $\theta$ -planes (region II). Downstream of the particle (region III), disks preferentially align with the  $r$ - $\theta$  planes with their axis of symmetry pointing along the azimuth. As for rods, the region III is divided into two subregions: in IIIa,  $\hat{\phi}$  is an attractive spiral, in IIIb it is an attractive node.

The splitting of the fluid flow into the regions shown in figures 3(b), (c) is a quasi-static characterization of the dynamical system (3), with micro-organisms held fixed at a given position in the flow. However, a non-motile micro-organism that is advected by the flow may be significantly displaced during the time it takes to achieve a given asymptotic orientation. To get further insight into equation (3), we compare the two timescales characterizing the advection and shear-induced reorientation. For simplicity, we combine the three timescales  $\tau_{I,II,III}$  associated with convergence onto the asymptotic solutions to equation (3b) into a single reorientation timescale  $\tau_r^{-1} \sim F \sim \|A\|_2$ . We estimate the advective timescale  $\tau_a \sim R/\|v\|$  at a given position as the time needed to travel the distance  $R$  at the local speed  $\|v\|$ . Figure 3(d) shows the ratio  $\tau_a/\tau_r$  as a function of the position. In particular, in the bright oval near the particle  $\tau_a > \tau_r$ , indicating that, in that region, non-motile bacteria advected by the flow have enough time to orient under the fluid forces in the manner outlined in figures 3(b), (c) for immobilized bacteria.

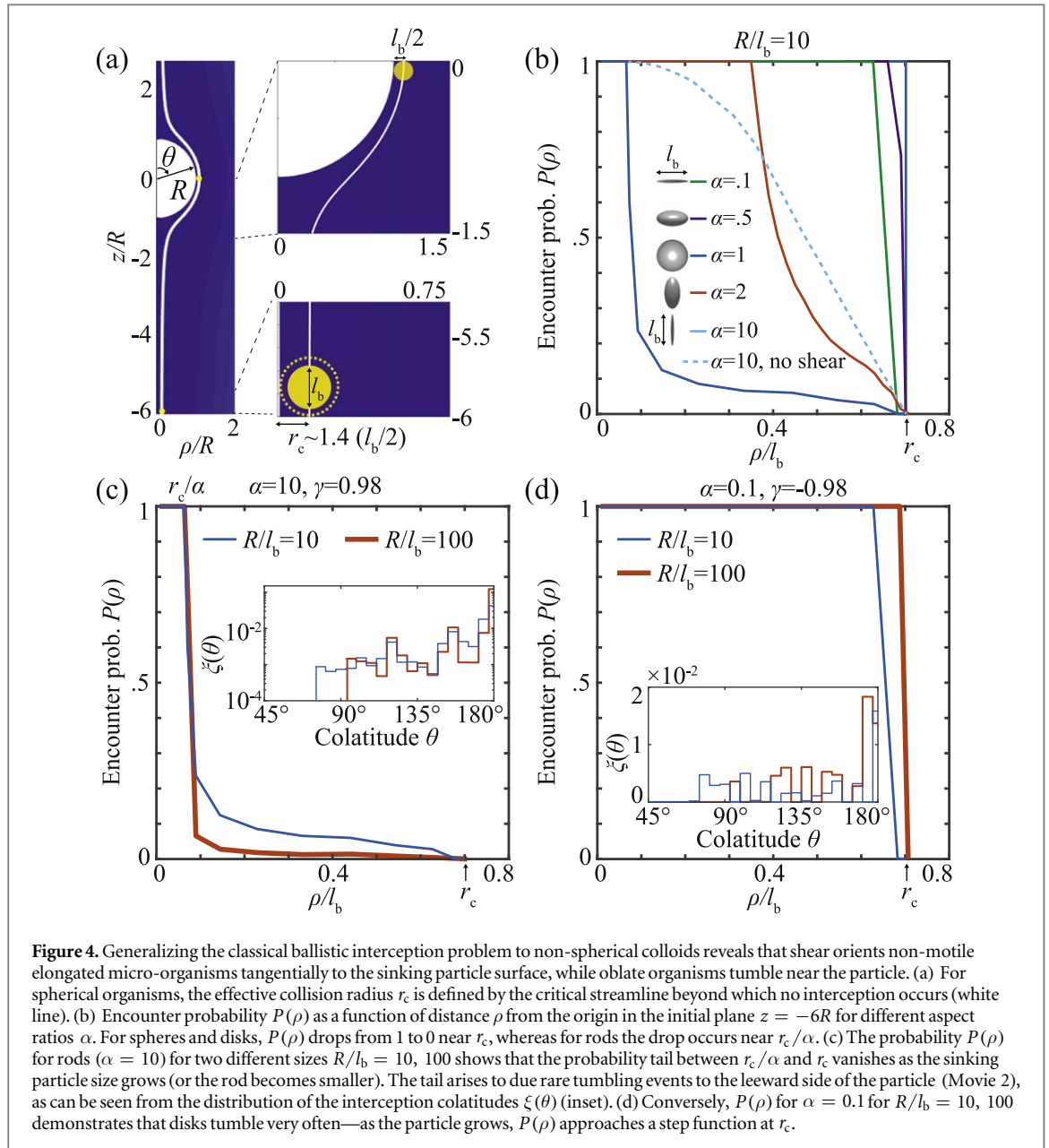
Finally, we note that the eigenvalues of the velocity gradient  $A$  (13) on the stagnation line ( $\theta = 0, \pi$ ) and the particle surface ( $r = 1$ ) have multiplicity greater than one. In this case, the analysis of section 3.1 does not directly apply, yet these special locations are important for the encounter process of non-motile micro-organisms, which can only approach the sinking particle near the stagnation line  $\theta = \pi$ . In appendix A.4, we show that on the upstream stagnation line ( $\theta = \pi$ ) rods align tangentially to the sinking particle, while on the downstream stagnation line ( $\theta = 0$ ), rods align vertically. This picture can be inferred from figure 3(b) by taking the limit  $\rho \rightarrow 0$ . Similarly, disks align tangentially to the particle surface for  $\theta = \pi$  (with axis of symmetry in the vertical direction), while they lie in the  $r - \theta$  plane for  $\theta = 0$ . Therefore, non-motile rods or disks approaching the sinking particle along the  $\theta = \pi$  stagnation line orient with their longer dimension tangential to the particle surface. Furthermore, on the particle surface, shear maintains to zeroth order the tangential orientation of rods and disks as they are advected around the sinking particle (appendix A.4). This suggests that it is the shorter dimension of rods and disks that determines their collision with the particle. However, for any finite size micro-organism, one must step away from the stagnation line and the particle surface. In the vicinity of these degenerate sets, the response is captured in figures 3(b), (c). The asymptotic orientations rods and disks assume in their respective regions I suggest that the tangential orientation prevails. However, in regions II and III shear reorients rods and disks away from the tangential orientation. Given the size of the regions II and III for rods and disks, this reorientation should be stronger for disks, since disks experience it over a larger part of the particle surface. In the next section, we use numerical simulations to confirm this intuition: the collision radius of rods is determined by their width, not length, whereas for disks the collision radius is determined by the longest dimension.

## 4. Non-motile bacteria and diatoms

Understanding the interception of non-motile elongated and oblate micro-organisms by a sinking particle is important for two reasons. First, in its own right, because many marine micro-organisms including many bacteria and phytoplankton species are non-motile and come in a variety of shapes, with bacteria often being spherical or elongated and phytoplankton being either elongated (e.g. chains), spherical or disk-like (e.g. diatoms). Second, the non-motile case corresponds to the high sinking speed limit  $U/U_b \rightarrow \infty$  for motile bacteria. We predict drastically different encounter rates for rods and disks: rods are particularly inefficient at intercepting the sinking particle due shear, which aligns them in the direction tangential to the particle surface (section 4.1). Conversely, disks eventually tumble under shear and explore their long axis to reach the collector. Experiments on elongated diatoms support this picture (section 4.2).

### 4.1. Interception of non-motile bacteria

The ballistic interception of non-motile micro-organisms by a sinking particle is conceptually identical to the classical problem of filtration, in which a colloid is captured by a large collector [9]. Previous works focused on spherical colloids; through numerical simulations, we extend these results to non-spherical colloids. Rods and disks, such as certain species of bacteria or diatoms, have drastically different effective collision radii. Due to shear-induced reorientation, the collision radius for a rod is determined by its width rather than length, while disks explore their full size to intercept the collector.



First, we briefly review the classical interception of small non-motile spherical beads by a large spherical collector. The reorientation of beads under the flow does not affect the interception problem, which reduces to identifying the streamline of closest approach (figure 4(a)). For the Stokes flow (2), the stream-function is given by

$$\psi(r, \theta) = \frac{1}{2}Ur^2 \left( 1 - \frac{3}{2}R/r + \frac{1}{2}(R/r)^3 \right) \sin^2 \theta. \quad (17)$$

The streamlines determined by equation (17) have the fore-aft symmetry, which implies that the critical streamline separating captures from misses is defined by the point  $r = R + l_b/2$  and  $\theta = \pi/2$ . Tracing the streamline upstream from this point to  $z = -6R$ , where we start the simulations, defines the effective collision radius  $r_c$ . For a spherical bacterium with  $l_b/R = 1/10$ , the collision radius is  $r_c \approx 1.4(l_b/2)$ ; the additional 40% arise due to the squeezing of the streamlines near the collector. Had we traced the streamline all the way to  $z \rightarrow -\infty$ , the prefactor would change from 1.4 to 1.2 [9]. In general,  $r_c$  depends very weakly on the size of spherical bacteria  $l_b/R$  and the formula  $r_c \approx 1.4(l_b/2)$  works very well for the bacterial sizes in the range  $0 < l_b/R < 1/10$ . Finally, for spherical colloids, the effective collision radius and the encounter efficiency (equation (7)) are related as

$$\eta_{\text{spheres}} = (r_c/R)^2. \quad (18)$$

We now turn to non-spherical organisms, for which the orientational dynamics can no longer be neglected.

As non-spherical micro-organisms follow the streamlines, they can intercept the sinking particle using either their shorter or longer dimension. Two extreme scenarios are possible: an organism always aligns its longer side tangentially or perpendicular to the particle, which modifies its collision efficiency by a factor of  $\alpha^2$ . Assuming negligible rotational diffusion, shear impacts the orientation of non-spherical organisms only through the aspect ratio  $\alpha$ . This follows from non-dimensionalizing equations (3) with  $U_b = 0$  in terms of the particle radius  $R$  and timescale  $R/U$ . However, while the organism size  $l_b$  does not directly affect the dynamics, it determines the interception criterion: we take the sinking particle to be a perfect absorber and stop simulations if any part of the rod or disk touches the particle (appendix A.5). We now systematically vary  $\alpha$  and  $l_b/R$  and measure the encounter probability and typical interception location.

The impact of the micro-organism aspect ratio  $\alpha$  and its relative size  $l_b/R$  on the encounter problem is summarized in figures 4(b)–(d);  $l_b$  denotes the longer dimension—length for elongated organisms, width for oblate ones. Varying  $\alpha$  (figure 4(b)) at fixed  $R/l_b = 10$ , shows that the collision radius of elongated micro-organisms is determined by their width, not length (Movie 1). This is evident from the variation of  $P(\rho)$ , the interception probability for an initial position at distance  $\rho$  from the centerline:  $P(\rho)$  decreases sharply from one once  $\rho > r_c/\alpha$ . The probability tail between  $r_c/\alpha < \rho < r_c$  indicates that rods occasionally reorient and use their length to intercept the particle (Movie 2). However, shear largely suppresses this effect, see the light blue broken line in figure 4(b), which represents trajectories without the shear-induced reorientation (parallel transport). In contrast to elongated micro-organisms, oblate organisms (disks) utilize their full size to intercept the particle— $P(\rho)$  drops sharply from one to zero near  $r_c$ . To see the impact of varying the relative size  $R/l_b$ , we fixed two aspect ratios,  $\alpha = 10$  (figure 4(c)) and  $\alpha = 0.1$  (figure 4(d)) and computed  $P(\rho)$  as well as the distribution  $\xi(\theta)$  for  $R/l_b = 10, 100$ . We observe that, as the colloid gets smaller (or the sinking particle gets larger), the effects described above become more pronounced, in the sense that for rods the probability tail between  $r_c/\alpha < \rho < r_c$  shrinks, whereas for disks  $P(\rho)$  approaches a step function with jump at  $r_c$ . Therefore, the formula (18) for the encounter efficiency by spherical colloids is replaced by

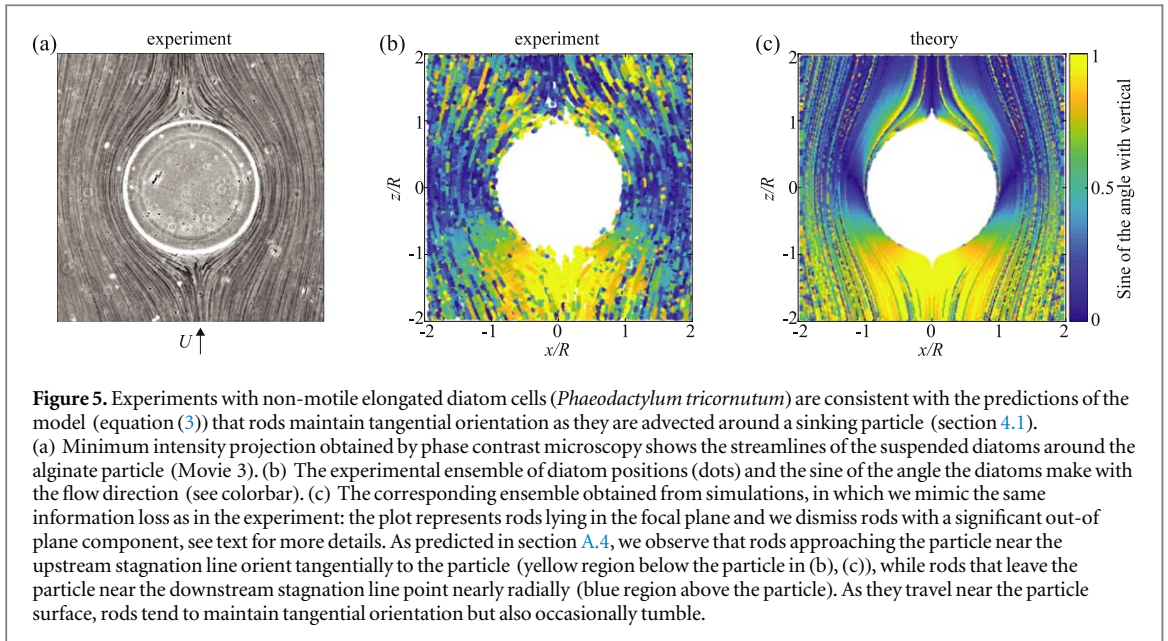
$$\eta_{\text{rods}} = [r_c/(\alpha R)]^2 = \eta_{\text{spheres}}/\alpha^2, \quad \eta_{\text{disks}} = \eta_{\text{spheres}} \quad (19)$$

in the case of (small  $R/l_b \gg 10$ ) non-spherical colloids, where rods means  $\alpha \gg 1$  and disks  $\alpha \ll 1$ .

Different interception efficiency for rods but not disks as compared to spherical colloids is consistent with the analytical arguments presented in section 3.2. Initially, shear aligns rods and disks tangentially to the sinking particle surface as they approach it along the stagnation line (regions I in figures 3(b), (c)). As they slide near the particle, both rods and disks experience shear that tries to reorient them away from the tangential configuration, potentially increasing their chance to intercept the particle (region II in figure 3(b) for rods and regions II and IIIa in figure 3(c) for disks). However, disks are exposed to this reorienting effect over a larger region than rods, suggesting that disks complete this reorientation while near the particle, whereas rods orient radially only when they are too far behind the particle (Movie 1). Occasional interception by rods caused by the reorientation in region II is responsible for the small probability tail in  $P(\rho)$  in figures 4(b), (c) (Movie 2). In summary, simulations confirm the intuition based on analytical arguments: the collision cross-section for rods is determined by their shorter dimension whereas the opposite is true for disks.

#### 4.2. Experiments with elongated diatom cells

Selected experiments with non-motile diatom cells confirmed the predictions of the model (3) discussed in sections 4.1, A.4 in the case of the non-motile rods (figure 5 and Movie 3). We ran a suspension of the non-motile, elongated diatom cells *Phaeodactylum tricornutum* (strain CCMP2561) in sea water at a mean flow velocity of  $168 \mu\text{m s}^{-1}$  through a microfluidic channel with a calcium-alginate spherical particle held fixed in the middle by the channel walls (figure 5(a)); see appendix A.6 for more details on the experimental protocol. The particle size was  $R = 566 \mu\text{m}$ , the average diatom length  $l_b = 21.2 \mu\text{m}$  and their average aspect ratio  $\alpha = 6.8$ . Rather than directly estimating the encounter rate, which proved difficult due to the challenge of imaging in the immediate vicinity of the particle, we used image analysis to quantify the orientation that the diatoms assume in the vicinity of the particle in the channel mid-plane. Using this approach, we extracted from 50 consecutive frames an ensemble of diatom positions and orientations (figure 5(b)). Since the shear-induced reorientation effects are strongest near the particle (figure 3(d)), we focused on diatoms that are at distance  $R < r < 2R$  away from the particle center. Importantly, since we only imaged the focal plane, this ensemble was skewed towards diatoms moving in the focal plane and also oriented in that plane. For this reason, to compare the experimentally determined orientations with those predicted by the model (3), we ran additional numerical simulations to mimic the same information loss as in the experiments. Specifically, we simulated a front of uniformly distributed and randomly oriented elongated non-motile rods (with  $R/l_b = 21.2$  and  $\alpha = 6.8$ ), as in the previous section. We focused on trajectories lying in the particle mid-plane (as in the imaged region) and extracted the rod orientations at positions along the streamlines corresponding to equal time intervals. We rejected orientations that have the out-of-plane component larger than  $\sin(30^\circ) = 0.5$ , to mimic the



information loss of diatoms that point out of the focal plane in experiments; the results were robust against variation in this threshold (figure A1).

The experimentally determined orientations of diatoms agreed very well with the numerical results for elongated ellipsoids with the same geometrical characteristics (figures 5(b), (c)). In particular, as predicted in appendix A.4, diatoms approaching the particle near the upstream stagnation line oriented tangentially to the particle surface, while diatoms departing from the particle near the downstream stagnation line pointed nearly radially (yellow versus blue regions in figures 5(b), (c)). Close to the particle surface, diatoms tended to maintain tangential orientation but can also occasionally tumble. Tumbling happened most often when diatoms were to the leeward side of the particle, which is consistent with the action of shear depicted in region II in figure 3(b), where vorticity dominates over straining and tries to spin rods in the plane of the picture. In summary, these experiments validate detailed aspects of our model for non-motile micro-organisms and demonstrate that the effect of shear—shape coupling can be substantial for realistic marine micro-organisms.

## 5. Motile bacteria

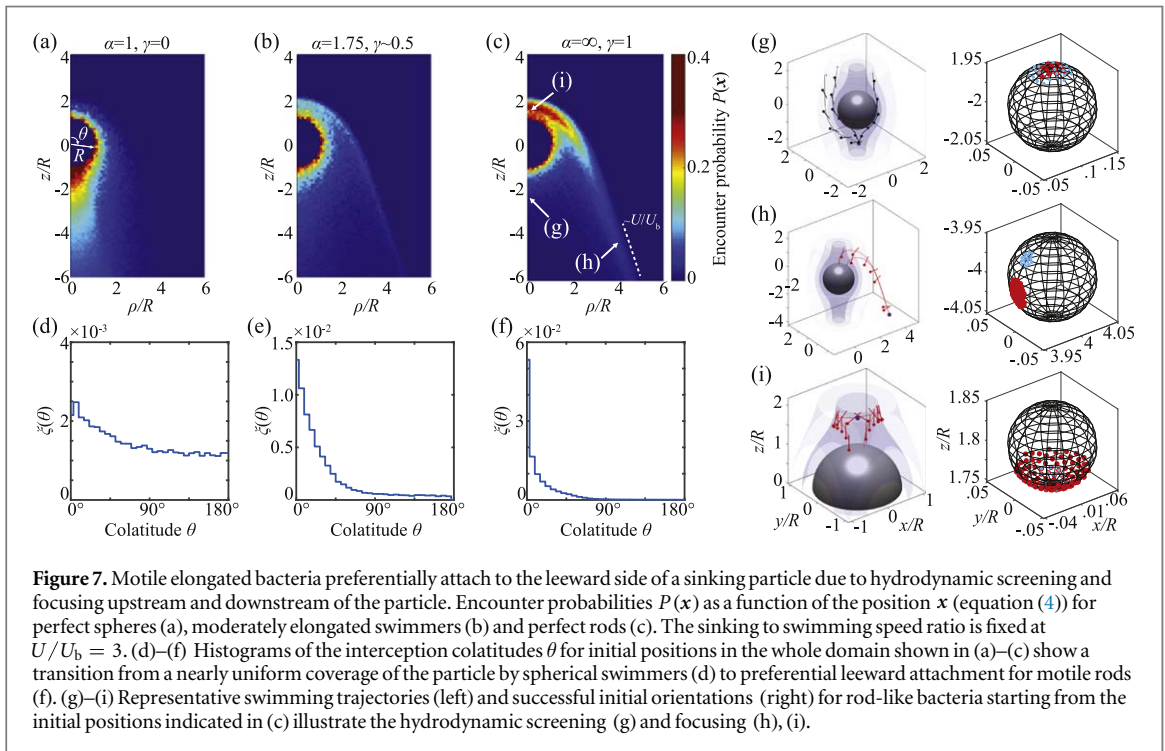
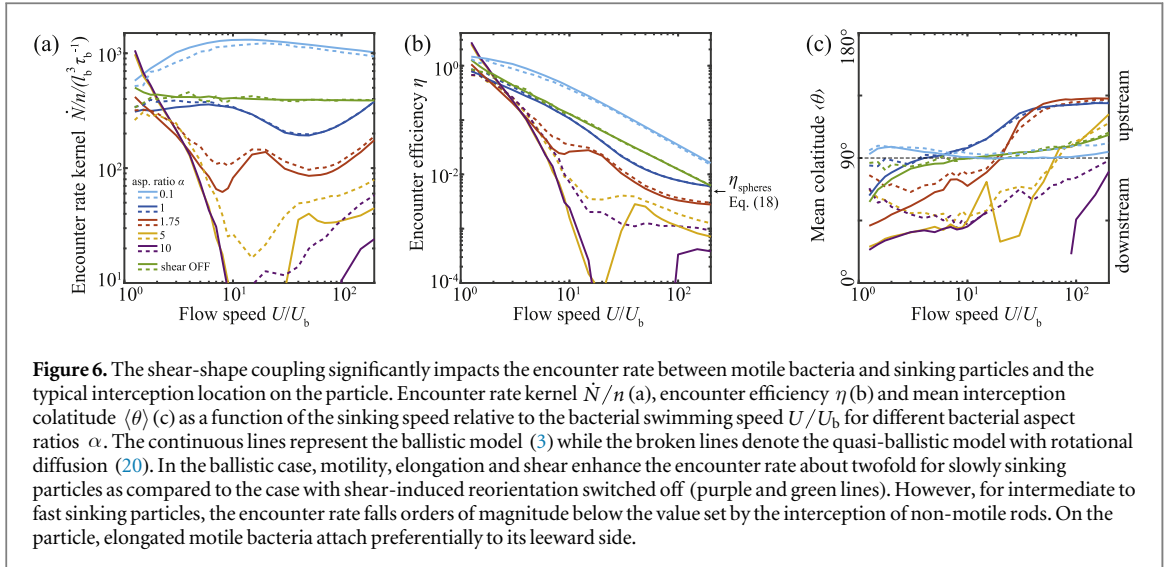
The encounter rate between motile elongated bacteria and sinking particles in the ballistic regime depends strongly on the particle sinking speed relative to the bacterial swimming speed (section 5.1). For slow sinking particles, shear increases the encounter rate more than twofold and leads to preferential attachment of bacteria to the leeward side of the particle. However, as the sinking speed increases, shear decreases the encounter rate, orders of magnitude below the rate of non-motile organisms. These mechanisms of hydrodynamic focusing and screening are rationalized at the level of individual bacterial trajectories (section 5.2) in terms of the quasi static picture derived in section 3. Finally, to connect with the diffusive description of the encounter process, we introduce rotational diffusion to quantify how various stochastic mechanisms, such as Brownian motion or run-and-tumble reorientation, influence the above ballistic description (section 5.3).

### 5.1. Encounter rates for motile bacteria

Nondimensionalization of the ballistic model (3) in terms of the particle radius  $R$  and the time scale  $R/U$  derived from the sinking speed  $U$  shows that the only two dynamically relevant variables are the ratio of the sinking to swimming speeds  $U/U_b$  and the bacterial aspect ratio  $\alpha$ . The bacterial size  $l_b$  and particle size  $R$  enter the problem through the interception condition but otherwise they do not affect the bacterial trajectories, except for the time it takes to execute them. We assume the particle is a perfect absorber and stop the simulations either if any part of the bacterium touches the particle (interception) or the bacterium ends up far behind the particle. In this section, we fix  $R/l_b = 10$ , scan velocities in the range  $U/U_b > 1$  (sinking speed greater than swimming speed) and consider several aspect ratios  $\alpha$  (figure 6).

For hypothetical spherical or oblate motile bacteria [22], the encounter rate kernel  $\dot{N}/n$  depends weakly on the sinking velocity  $U/U_b$  and the encounter efficiency  $\eta$  decays monotonically with  $U/U_b$ ; for spherical swimmers,  $\eta$  is close to the values obtained with the reorientation by shear switched off (dark blue and green





lines in figures 6(a), (b)). However, for elongated swimmers,  $\eta$  varies strongly with  $U/U_b$  (figures 6(a), (b)). For slowly sinking particles ( $1 < U/U_b < 2$ ),  $\eta \sim 2-3$ , implying that the particle collects bacteria from the volume of water two-three times bigger than the geometric cylinder the particle swipes as it sinks. Furthermore, elongated bacteria intercept the particle to the leeward side (figure 6(c)). Interestingly, as the sinking speed increases, the encounter rates drop very rapidly: in the velocity window  $10 < U/U_b < 100$ , the encounter rate of elongated swimmers ( $\alpha \geq 5$ ) can be orders of magnitude below the value set by the non-motile rods. We next rationalize these encounter rate enhancement and decrease using the concepts of hydrodynamic focusing and screening.

## 5.2. Hydrodynamic focusing and screening

The strong dependence of the encounter efficiency on the particle sinking speed for elongated bacteria (figure 6(b)) is a consequence of hydrodynamic focusing and screening. These phenomena are illustrated in figure 7, where we compare three swimmers with different aspect ratios; the sinking speed is fixed at  $U/U_b = 3$ . Figures 7(a)–(c) show the encounter probabilities  $P(\mathbf{x})$  for a bacterium starting at  $\mathbf{x}$  anywhere inside the indicated domain (not just the plane  $z = -6R$ ) with head pointing in a random direction (equation (4)). Since  $U/U_b > 1$ , in all three cases there is a cone-like surface of revolution that separates the accessible [ $P(\rho) > 0$ ] and inaccessible initial positions—if the

bacteria start too far away, they cannot reach the particle. The distribution of  $P(\mathbf{x})$  inside the accessibility region vary strongly with  $\alpha$ . For spheres,  $P(\mathbf{x})$  is concentrated below the particle, near the  $\rho = 0$  stagnation line and decays monotonically to zero with  $\rho$  reaching the accessibility horizon (figure 7(a)). For somewhat elongated swimmers  $\alpha = 1.75$ , the initial positions below the particle become less likely to result in an interception and  $P(\mathbf{x})$  starts to concentrate near the edge of the accessible region, which also reaches further out (figure 7(b)). For perfect swimmers  $\alpha = \infty$ , the region  $\rho \approx 0$  is now almost entirely shielded, with  $P(\mathbf{x})$  exhibiting a clear high-probability belt at the edge of the accessible region (figure 7(c)). Far below the particle, the belt slope approaches  $\sim U/U_b$ . Considering the distribution of the interception locations  $\xi(\theta)$  for initial positions anywhere in the domains shown in figures 7(a)–(c), elongated swimmers show preferential leeward attachment, with the vicinity of the ‘north pole’ being the most likely location (figures 7(d)–(f)). We now rationalize the shape of the distributions  $P(\mathbf{x})$  and  $\xi(\theta)$  at the level of individual swimming trajectories by evoking the quasi-static picture discussed in section 3.2 and shown in figure 3.

At the level of individual swimming trajectories, the probability  $P(\mathbf{x})$  for spherical swimmers (figure 7(a)) is realized by trajectories that correspond to swimmers initially located below the particle and pointing upwards. However, this intuitive strategy is not available for elongated swimmers because of hydrodynamic screening (figures 7(b), (c)). Recall that, below the particle, shear tends to align rods along the azimuth (region I in figure 3(b)). This shear-induced reorientation coupled with forward motility implies that rod-like swimmers get reoriented and swim away as they approach the sinking particle from below (figure 7(g), Movie 4). For the same reason, it is very unlikely that elongated swimmers attach to the front of the particle, which explains the small values of  $\xi(\theta)$  for colatitudes  $\theta > 90^\circ$  (figure 7(f)). Instead, successful interceptions for elongated bacteria must follow a different strategy (figures 7(h), (i)). To avoid the screening, elongated swimmers must start on the belt far away from the centerline of the sinking particle, on the edge of the accessibility horizon. Furthermore, their initial orientations have to be roughly horizontal, pointing towards the centerline (figures 7(h)). Such initial conditions allow the bacteria to avoid the screening region I of figure 3(b) and explore the shear-induced radial reorientation in region III. This hydrodynamic focusing then leads to preferential leeward attachment (Movie 5).

The mechanisms of hydrodynamic focusing and screening described above rationalize the strong dependence of the encounter efficiency  $\eta$  on the particle sinking speed  $U/U_b$  presented in (figure 6(b)). For slowly sinking speeds, both mechanisms are present. However, the high probability belt at the edge of the accessibility horizon for elongated swimmers extends a large volume and hence many swimmers can utilize the focusing effect, which explains why  $\eta > 1$  in that flow range. However, as  $U/U_b$  increases, the high probability belt moves closer to the center line since its diameter scales as  $U_b/U$ . This reduces the accessible volume of water at the rate at least  $\sim U^{-2}$ . Furthermore, as the belt shrinks in diameter, it enters the region of hydrodynamic screening and eventually disappears (figure A4(a)). Thus, in the range  $10 < U/U_b < 100$ , only screening persists, which explains the very small values of  $\eta$  in that range. Only for swimming speeds  $U/U_b > 100$ ,  $\eta$  rises again, until it starts to recover the limit set by the interception rate of non-motile rods.

### 5.3. Impact of rotational diffusion

In the purely ballistic picture of the encounter process outlined in the two previous sections, shear is the only factor responsible for micro-organism reorientation. In reality, bacteria experience Brownian rotational diffusion as well as perform run-and-tumble or run-and-reverse dynamics. The combination of these stochastic mechanisms likely interferes with the shear-induced reorientation in a complex manner. As a first step to systematically study the impact of these additional mechanisms, we introduce a single rotational diffusion term to equation (3)

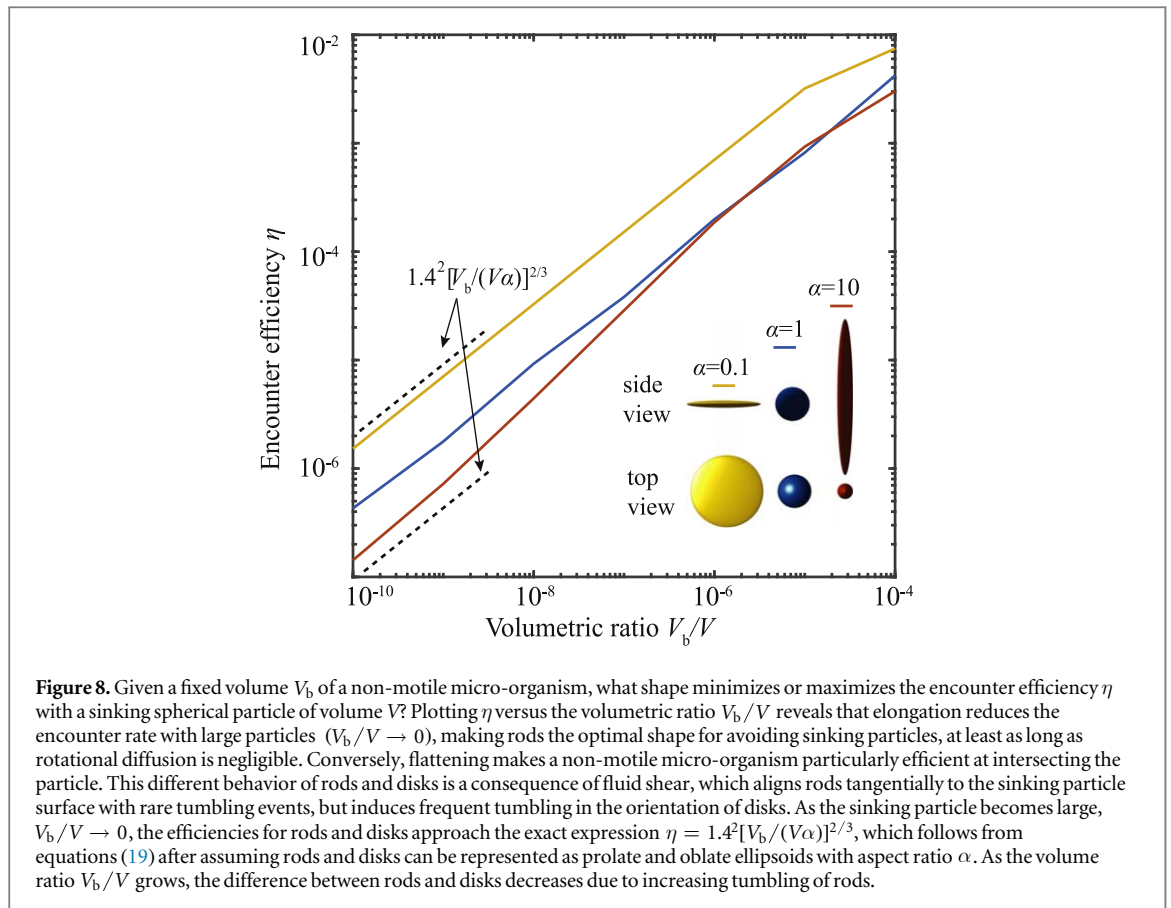
$$\dot{\mathbf{x}} = U_b \mathbf{p} + \mathbf{v}, \quad (20a)$$

$$\dot{\mathbf{p}} = (\mathbf{I} - \mathbf{p}\mathbf{p}^T)[(\gamma\mathbf{E} + \mathbf{W})\mathbf{p} + \sqrt{2D_r}\boldsymbol{\xi}], \quad (20b)$$

where  $D_r$  is the cell’s effective rotational diffusivity and  $\boldsymbol{\xi}$  is a delta-correlated 3D white noise with zero mean. We express the diffusive timescale  $\tau_d = D_r^{-1}$  in terms of the time  $\tau_b = l_b/U_b$  needed for a bacterium to travel the distance equal to its bodylength.

To study the impact of rotational diffusion on the encounter rates and attachment location, we fixed the diffusive timescale at  $\tau_d/\tau_b = 100$ , which corresponds to the typical time-scale set by the run-and-tumble motility [8]. We then repeated the scans according to the same protocol as in section 5.1, with  $R/l_b = 10$  and  $U/U_b > 1$  (the broken lines in figure 6). We find that diffusion has little effect on the encounter rates and attachment location for spherical swimmers. However, for elongated swimmers, diffusion decreases the impact of hydrodynamics focusing at low sinking speeds but also decreases the hydrodynamic screening at higher sinking speeds (see appendix A.7).





## 6. Discussion

In this work, we have studied the ballistic limit of the encounter process between micro-organisms and sinking particles, with focus on the reorienting effect of shear induced by the sinking particle. Analytical and numerical calculations as well as selected experiments show that the shear—shape coupling acting on a micro-organism impacts population-level observables, such as the encounter rate with sinking particles or the typical attachment location on the particle. For the Stokes flow around a spherical sinking particle, rods and disks break the fore-aft symmetry of the flow streamlines, in stark contrast to the behavior of spherical colloids (figure 3). This shape-induced symmetry breaking affects the encounter rates (figures 4 and 6) through mechanisms we have characterized as hydrodynamic focusing and screening (figure 7). Below, we first rephrase these results as solutions to the optimization problem: should a micro-organism be elongated or flat, to maximize or minimize the encounter rate with a large moving sphere? Subsequently, we discuss the biophysical consequences of our mechanistic description of the encounter process in the marine environment.

From the perspective of evolution, there are many contexts in which micro-organisms may seek to maximize or minimize their encounters with moving objects, including encountering sinking resources [8] or symbiotic partners [23], and avoiding predators [24]. At the same time these, micro-organisms are likely to have other constraints on their volume, such as growth maximization and genome size. For non-motile micro-organisms with negligible rotational diffusion (section 4.1), we have seen that shear tends to orient rods tangentially to the sinking particle surface as these move around the particle, whereas disk-shaped micro-organisms tumble, which makes their longer dimension available for interception (section 4.1 and figure 4). As a consequence, rods have their encounter efficiencies decreased by a factor equal to the square of their aspect ratio compared to spherical colloids with diameter equal to the rod length. Conversely, disks have the same efficiency as spheres with diameter equal to the disk diameter (equations (19)).

For non-motile bacteria, over a broad range of ratios of cell volume relative to particle volume ( $V_b/V$ ), disks are the most efficient shape to intercept a sinking particle, while rods are the least efficient (figure 8). The contribution of the occasional tumbling of rods grows with  $V_b/V$ , decreasing the difference between the efficiencies of rods and disks as cell volume gets larger; rods remain less efficient than disks but catch up with spheres. Note that we cannot increase the volumetric ratio further without violating the approximations used in the Jeffery equation, since the micro-organism size becomes comparable with the sinking particle. Conversely,

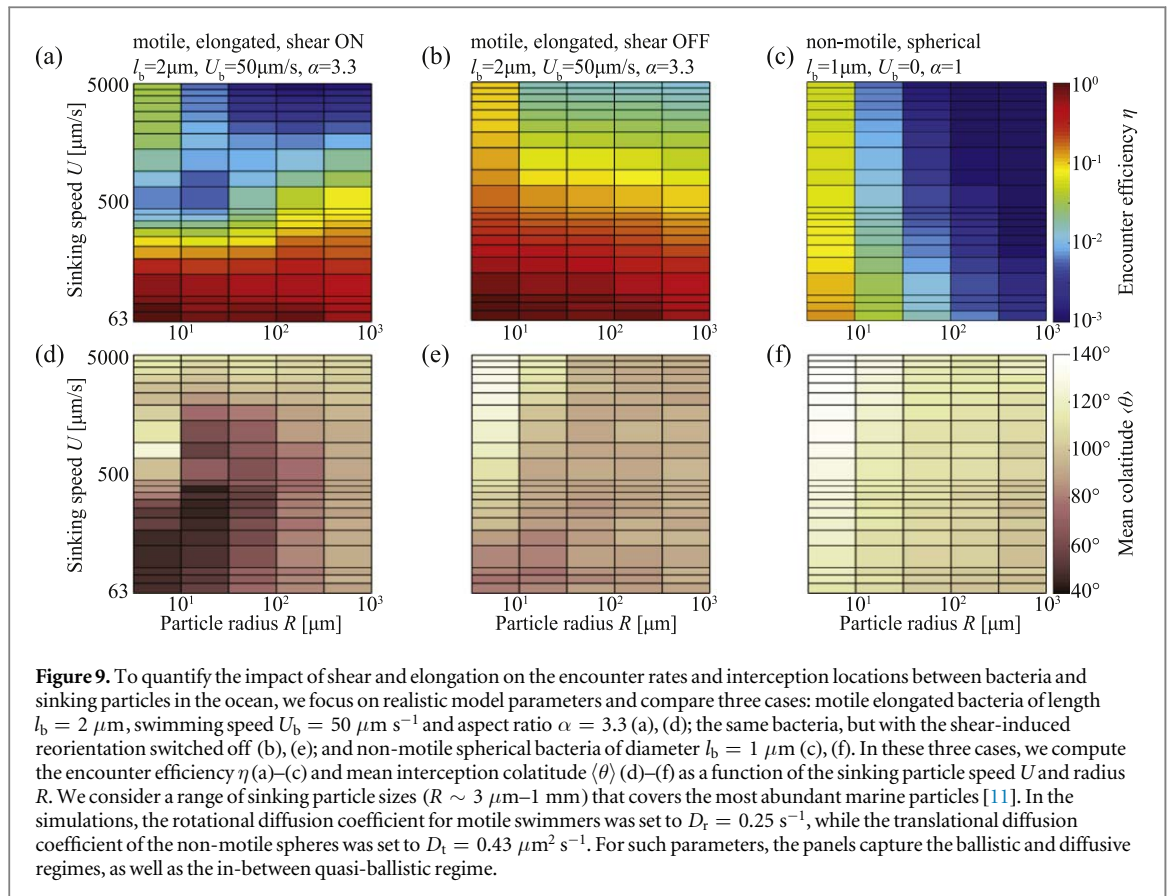
as the sinking particle grows,  $V_b/V \rightarrow 0$ , the encounter efficiencies approach  $1.4^2[V_b/(V\alpha)]^{2/3}$  (broken lines in figure 8), which follows directly from equations (19) and reflects the fact that, as the sinking particle grows, rods cease to tumble while disks always tumble (figures 4(c), (d)). In this limiting regime, the efficiency ratio between disks and rods is  $(\alpha_{\text{rod}}/\alpha_{\text{disk}})^{2/3}$ . For example, for rods with  $\alpha_{\text{rod}} = 10$  and disks with  $\alpha_{\text{disk}} = 0.1$ , disks will be about 20 times more efficient than rods at intercepting large sinking particles.

For motile micro-organisms, encounter rates are controlled by hydrodynamic focusing and screening, which develop from the influence of shear on the direction of swimming. Here we still consider the ballistic regime, with negligible rotational diffusion. In addition, the shear—shape coupling for motile cells leads to the sensitive dependence of the encounter rate on the particle sinking speed relative to the bacterial swimming speed (section 5.1 and figure 6). Hydrodynamic screening and focusing describe the effect on elongated motile micro-organisms of the shear upstream and downstream of the particle, respectively. In hydrodynamic screening, the shear upstream of the particle aligns rods tangentially to the particle surface (as with non-motile cells), resulting in cells swimming away from the particle. For hydrodynamic focusing, rotation from shear in the downstream half of the particle turns the swimming rods towards the particle. For slowly sinking particles, focusing dominates and enhances the encounter rate (figure 7), while at sinking speed significantly higher than the cell swimming speed, screening dominates and the encounter rate drops far below that of non-motile rods. In contrast to elongated organisms, hypothetical spherical and disk-shaped swimmers respond monotonically to changes in the sinking speed (figure 6), a consequence of disk-shaped swimmers experiencing hydrodynamic focusing upstream, not downstream, of the particle. For sinking speeds more than twice the swimming speed, this results in disk-shaped micro-organisms encountering particles at a higher rate than elongated micro-organisms.

From an evolutionary perspective, this analysis suggests that adopting a disk shape would be optimal for micro-organisms (whether non-motile or motile) in order to maximize particle encounter rates at a broad range of sizes and sinking speeds. Of course, this neglects other evolutionary pressures on morphology. However, for particles sinking at speeds close to the organism swimming speeds (i.e. relatively slowly), elongation increases the encounter rates up to twice that of motile disks. Coupled with the large reduction in encounter rates for more rapidly sinking particles, elongation can be viewed as biasing ballistically swimming organisms strongly towards slowly sinking particles. This could be subject to selective pressures for micro-organisms in situations where optimal growth occurs near the surface, and therefore rapidly sinking particles are better avoided.

For the specific case of marine bacteria encountering sinking marine particles, it is necessary to connect the ballistic description of the encounter process with the classical approach based on approximating bacterial motility as a diffusive process [7, 8, 25]. Marine bacteria are subject to various sources of random reorientation, from Brownian rotational diffusion to self-generated run-and-tumble or run-and-reverse motility, where segments of straight swimming are interrupted by randomization of the swimming direction. As a consequence, on scales larger than the bacterial run length and timescales longer than the reorientation time, bacterial motility can be effectively characterized as a diffusive process [7, 8, 25]—this is a general feature of superimposing a large number of uncorrelated random segments [26]. In this limit, relevant to large sinking particles, the encounter rate is proportional to the bacterial effective diffusion coefficient and the Sherwood number, a flow-induced enhancement factor [25]. Additionally, while the shear-induced reorientation in the diffusive limit can be neglected in certain regimes [12], precise quantification of its impact on the encounter rate and attachment locations across a wide range of particle speeds and sizes might require kinetic theory approach [26–28]. However, as the particle becomes smaller or the sinking speed increases, the system becomes ballistic and the diffusive approximation overestimates the encounter rate. The reason for this overestimation comes from the fact that the encounter probability for a bacterium at distance  $r$  from the particle decays as  $r^{-1}$  in the diffusive regime, and as  $r^{-2}$  in the ballistic regime [29], at least for stationary particles and without shear. Since hydrodynamic interactions can significantly bend bacterial trajectories [14, 30, 31], the need to go beyond arguments based on straight-line swimming motivated the above study of the pure ballistic limit. For the marine application, we consider ballistic motile bacteria supplemented by rotational diffusion (section 5.3), which we have shown reduces the strength of hydrodynamic screening on rod-shaped swimming cells.

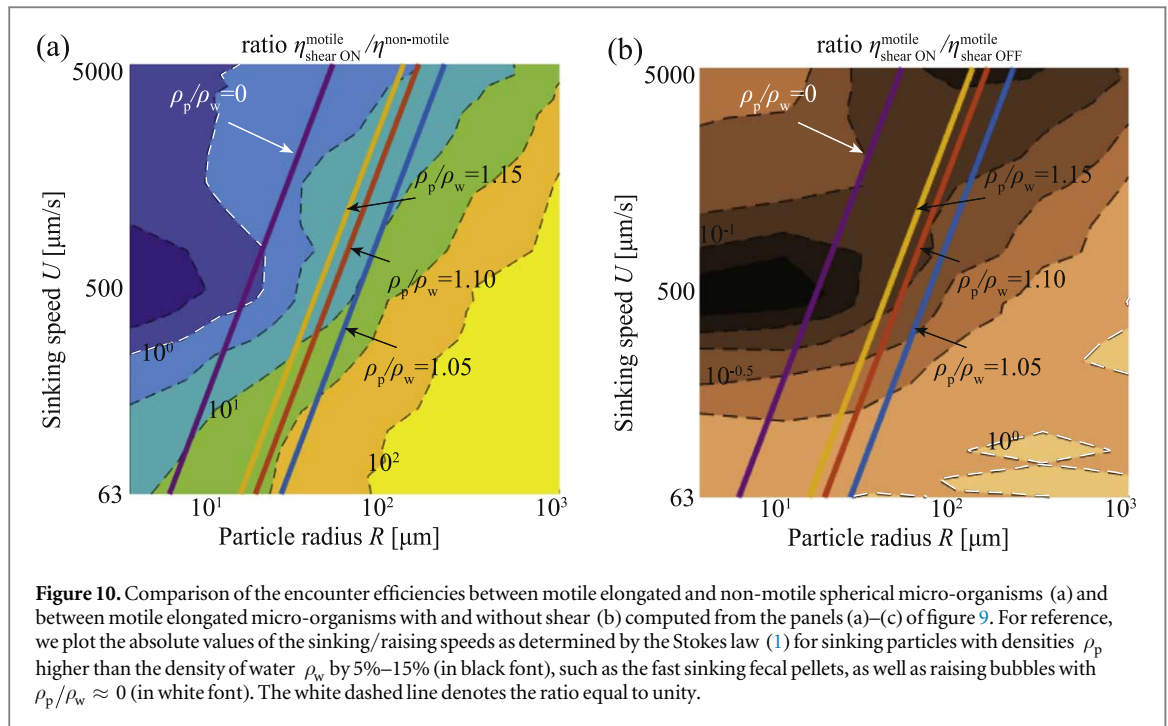
We consider two major classes [8]: motile elongated bacteria and non-motile spherical bacteria. For motile elongated bacteria, we evaluate the predictions of our model for cells of length  $l_b = 2 \mu\text{m}$ , swimming speed  $U_b = 50 \mu\text{m s}^{-1}$  and aspect ratio  $\alpha = 3.3$ . For non-motile spherical bacteria, we choose a diameter  $l_b = 1 \mu\text{m}$ . These represent typical characteristics of motile copiotrophic bacteria that actively seek and engage marine particles, and more oligotrophic non-motile bacteria which may nevertheless encounter and stick to particles. For these representative marine bacteria, as well as the equivalent motile bacteria without the influence of shear, the corresponding encounter efficiency  $\eta$  (figures 9(a)–(c)) and mean interception colatitude  $\langle\theta\rangle$  (figure 9(d)–(f)) have been computed as a function of the sinking particle speed  $U$  and particle radius  $R$ . The range of sinking speeds we consider is  $60 \mu\text{m s}^{-1}$ – $5 \text{mm s}^{-1}$ . The range of particles sizes,  $3 \mu\text{m}$ – $1 \text{mm}$ , covers the most abundant marine sinking particles [11]. For elongated bacteria, randomization of orientation is effectively represented by a



single rotational diffusion coefficient  $D_r = 0.25 \text{ s}^{-1}$ ; the diffusive timescale ( $\sim 4 \text{ s}$ ) gives the run length of about  $200 \mu\text{m}$ , typical of marine bacteria [8]. For such a run length, the range of particle sizes spans the ballistic and diffusive regimes as well as the intermediate transition range. Finally, the translational diffusion of the non-motile spherical bacteria was set to  $D_t = 0.43 \mu\text{m}^2 \text{ s}^{-1}$ , which represents Brownian motion of a micron-sized sphere at room temperature [32]. Under these conditions, accounting for the shear reorientation of motile marine bacteria substantially reduces the encounter efficiency for small fast-sinking particles and alters the location of encounters for slow-sinking particles below  $100 \mu\text{m}$  in radius. In contrast, the diffusive spherical swimmers show weak dependence of encounter efficiency on sinking speed, but much greater sensitivity to particle size.

Since the range of particle sizes considered in figure 9 captures the ballistic-diffusive transition, the standard computation based on a diffusive analogy only matches the encounter rates of marine bacteria (neglecting shear) for the largest particles with radii approaching  $1 \text{ mm}$  (figure A2). For bacteria with higher rotational diffusivity, this occurs for smaller particle sizes. As the particles get smaller, the diffusion-based calculation starts to overestimate the encounter rate—in the ballistic limit, with particle sizes reaching tens of microns, the two descriptions can differ by more than two orders of magnitude (figure A2). We now describe in detail the encounter process in the intermediate quasi-ballistic regime, highlighting the role of bacterial motility and fluid shear.

Factoring in shear interactions, motile bacteria encounter sinking particles at a rate one or two orders of magnitude (figure 10(a)) greater than non-motile bacteria. This motility-based enhancement factor is smaller by one or two orders of magnitude (depending on particle size) as compared to what would be predicted by the fully diffusive model. The exception when motility decreases the chances of interception ( $\eta_{\text{shear ON}}^{\text{motile}} / \eta^{\text{non-motile}} < 1$ ) corresponds to small and very quickly moving objects. This upper-left part of the panel, close to the full ballistic regime, is dominated by hydrodynamic screening and is probably not relevant for marine particles, even for fast sinking-fecal pellets, since their density differs from that of seawater only by about 10%–20% [33, 34], see the red and yellow lines in figure 10, which represent the Stokes law (1). However, this hydrodynamic screening regime may be relevant for interception by air bubbles, whose vertical speed is high in view of their large density difference with seawater [35] (purple line in figure 10). Furthermore, comparing the shear on–off cases for motile elongated bacteria (figure 10(b)), we find that the major impact of shear is to reduce the encounter rates with small particles sinking at intermediate or rapid rates by up to a factor of 10. This reduction is a consequence of the competition between the hydrodynamic screening of rods upstream of the



sinking particle and rotational diffusion. It suggests that elongation-induced screening may be a passive mechanism that allows motile elongated marine micro-organisms to prioritize slowly sinking aggregates, at least in the quasi-ballistic particle size range.

For slowly sinking particles in the quasi-ballistic regime (lower parts of the panels in figure 10), the observed encounter efficiencies of motile marine bacteria are close to the case without shear, consistent with earlier studies [12]. However, at the level of individual trajectories, this encounter rate is realized by hydrodynamic focusing, which results in most bacteria attaching to the leeward side ( $\theta < 90^\circ$ ) of the sinking particle (compare figures 9(d) and (e); see also figure A3). For small and slowly sinking particles ( $R < 50 \mu\text{m}$ ,  $U < 500 \mu\text{m s}^{-1}$ ), for which shear dominates over rotational diffusion, more than 75% of the interceptions occur on the leeward side of the particle. Furthermore, about 25% of the interceptions are concentrated inside the ‘Arctic circle’ ( $\theta < 23^\circ$ ), which represents a more than five-fold increase as compared to a uniform coverage of the particle. This leaves the southern hemisphere depleted of bacteria, with almost no interceptions below the ‘tropic of Capricorn’ ( $\theta > 113^\circ$ ). Thus, the leeward stagnation point is a flow-induced hotspot where motile and elongated bacteria concentrate due to shear. Since non-motile bacteria intercept the particles on the upstream side (figure 9(f)), in the southern hemisphere, we conclude that flow and shear lead to a bipolar segregation of motile and non-motile marine bacteria on the two sides of a sinking particle.

Although this work has assumed particles to be spherical despite the variety of observed shapes exhibited by marine snow aggregates [11], we expect the phenomena of hydrodynamic focusing and screening of elongated bacteria to be robust to variation in shape. The focusing and screening effects rely on different orientational responses of small rods upstream and downstream of the particle—the key property of the flow that is required for this fore-aft symmetry breaking is the expansion of the streamlines to the front of the particle and their recombination to the back, as well as the no-slip boundary conditions on the particle surface. As long as such general streamline organization is preserved, the effects here described should be robust: while fluid parcels roll on the particle surface (no slip), they stretch upstream of the particle (streamline expansion) but compress downstream of the particle (streamline recombination). This basic process will hold for objects at low Reynolds numbers with no-slip surfaces, and one would therefore expect hydrodynamic focusing and screening of motile elongated bacteria to occur for marine particles in general.

## 7. Conclusions

In this work, we combined analytical and numerical calculations to estimate the encounter rates between non-motile and motile micro-organisms of different morphologies and sinking particles in the ballistic regime relevant for the most abundant small sinking particles. Previous estimates have primarily focused on the diffusive regime, effectively assuming that particles are much larger than the bacterial run length. In the ballistic range, bacterial reorientation becomes a significant factor influencing the encounter process, while it is absent by



necessity from diffusive models. We have focused on the coupling between micro-organism shape and fluid shear induced by the particle, since shear is the dominant external factor responsible for bacterial reorientation. We have shown that the shape—shear coupling can significantly affect the encounter rate and attachment location on a particle for both non-motile and motile micro-organisms.

For non-motile organisms, shear from a sinking particle can significantly alter the encounter rates of organisms with different morphologies. For elongated organisms, this influence occurs by aligning the cells' long axis tangentially to the particle surface, and was experimentally validated. When the timescale of rotational diffusion is long with respect to particle interactions, shear from sinking particles interacts with the aspect ratio of non-motile organisms to potentially reduce encounter rates by a factor proportional to the square of the aspect ratio. As a result, encounters could exert evolutionary pressure on non-motile cell morphology [36], favoring elongated or disk-like shapes depending on whether encounters are unfavorable or favorable, respectively.

For motile micro-organisms, interactions with the shear from a sinking particle give rise to two phenomena, hydrodynamic screening and focusing, that alter both the rates and locations of encounters. Elongation helps organisms intercept slowly sinking particles but dramatically reduces the encounter rate with rapidly sinking particles. In contrast to rods, motile disks experience upstream focusing, leading to high efficiency at intercepting rapidly sinking particles. From the perspective of the particle, motile elongated micro-organisms typically attach to the leeward side of the particle, while motile disks cover it more uniformly. Under realistic parameters relevant to marine bacteria and sinking particles, which include the effect of randomization of swimming direction from rotational diffusion, hydrodynamic screening leads to a ten-fold decrease in the interception rate of rapidly sinking aggregates, as compared to motility without the shear-induced reorientation. This reduction in encounter rate suggests that elongation-induced screening may be a passive mechanism that allows motile elongated marine micro-organisms to avoid rapidly moving particles. Last but not least, motile elongated bacteria attach to the leeward side of the particle, whereas non-motile bacteria attach to the front. Thus, hydrodynamic focusing is a physical source of heterogeneity in particle colonization characterized by bipolar segregation of motile and non-motile micro-organisms, which may influence the degradation rate of marine snow aggregates. Whether in terms of encounter rates or encounter locations, these results indicate that the impact of shear reorientation cannot be neglected when evaluating interactions between motile organisms and sinking particles.

The dynamics of shear-driven reorientation are directly relevant to the colonization of marine particles by bacteria. It is well established that motility can greatly enhance the encounter rate of bacteria with sinking particles [8, 24]. This enhancement is often estimated via the ratio of the effective diffusivity due to motility and the diffusivity due to Brownian motion, which can be as large as 1000 for highly motile marine bacteria [8, 37, 38]. The more accurate theory developed here, which accounts explicitly for the interaction between flow and motility in elongated bacteria, refines this estimation in a manner that depends on the particle size and sinking speed relative to the bacterial motility. For particles substantially larger than the bacterial run length, the enhancement in attachment due to motility estimated by the ratio of effective diffusivities and neglecting the impact of shear is increasingly more accurate. For the marine bacteria modeled here, this corresponds to particles with radius greater than approximately 1  $\mu\text{m}$ . For smaller particles, which form the bulk of particles in the ocean [39], this work reveals that the enhancement in encounters resulting from motility is more moderate and is further reduced as the particle sinking speed increases. In extreme cases, potentially applicable to some bubbles, motility may confer no benefit in encounter rates. However, in the context of marine particles, motility still enhances encounters by one to two orders of magnitude. Since the enhancement in encounter rate due to motility is greater for slowly-sinking particles, this also highlights the potential significance of neutrally buoyant particles [40] to motile bacteria. This fundamental knowledge of encounter rates will be a valuable asset in future efforts to rationalize the community composition on marine particles, and ultimately the role of different groups of bacteria in particle degradation and the ocean's biological pump.

In a different domain, the mechanisms of hydrodynamic focusing and screening of rods and disks here described are relevant to the classical filtration problem [9], because our results suggest that shear renders elongated non-motile colloids more difficult to collect than oblate ones. Furthermore, fabrication of Janus-type artificial swimmers makes it possible to build microscale motile objects with different shapes and swimming speed [32], and these parameters could be tailored to enhance or suppress the focusing and screening effects. For example, the efficiency in capturing moving spheres may be important in applications such as targeted drug delivery [41] and micromachine-enabled decontamination [42].

In summary, we have demonstrated that hydrodynamic interactions between a small ellipsoid and a large moving sphere break the fore-aft symmetry of the flow streamlines, leading to practical consequences for micro-organisms. This symmetry breaking is a consequence of fluid expansion and recombination upstream and downstream of the sphere, but is only revealed when the full tensorial character of the velocity gradient is accounted for, including its straining and rotational components. Such asymmetric two-body couplings are

ubiquitous, since they arise when a small non-spherical particle travels near a larger obstacle in a fluid; we have experimentally verified their impact in the case of non-motile elongated diatoms advected around an algininate bead. In the context of swimming bacteria intercepting a sinking particle, hydrodynamic focusing and screening have practical ecological impacts, but applications to other natural or man-made systems are yet to be explored.

## Acknowledgments

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## Appendix

The appendix is organized as follows: we provide linear stability analysis of the fixed points of the Jeffery equation in section A.1 and derive the limit cycle solutions and their period in section A.2; these results were discussed in section 3.1 of the Main Text. The velocity gradient for the Stokes flow is derived in section A.3; its matrix form was used in equation (13) in section 3.2 of the Main Text. In section A.4, we complement the discussion in section 3.2 of the Main text by analyzing the structure of the velocity gradient on the stagnation lines and the sinking particle surface. The subsequent sections give details on the numerical simulations (section A.5) and experimental methods (section A.6). Finally, the three additional figures supplement the Main Text as follows: figure A1 shows that the results presented in figure 5 of the Main Text are robust to variation in the cut-off threshold for rejecting the out-of-plane components of rods in the simulations, figure A2 quantifies the overestimate in the encounter efficiencies as predicted by the classical diffusive arguments in the range of parameters discussed in figures 9 and 10 of the Main Text, and figure A3 provides an additional characterization of the landing distributions for the simulations presented in figure 9 of the Main Text.

### A.1. Stability analysis of the fixed points of the Jeffery equation

In this section, we analyze the linear stability of the fixed points of the Jeffery equation (9)

$$\dot{\mathbf{p}} = (\mathbf{I} - \mathbf{p}\mathbf{p}^T)\mathbf{A}^T\mathbf{p}. \quad (\text{A1})$$

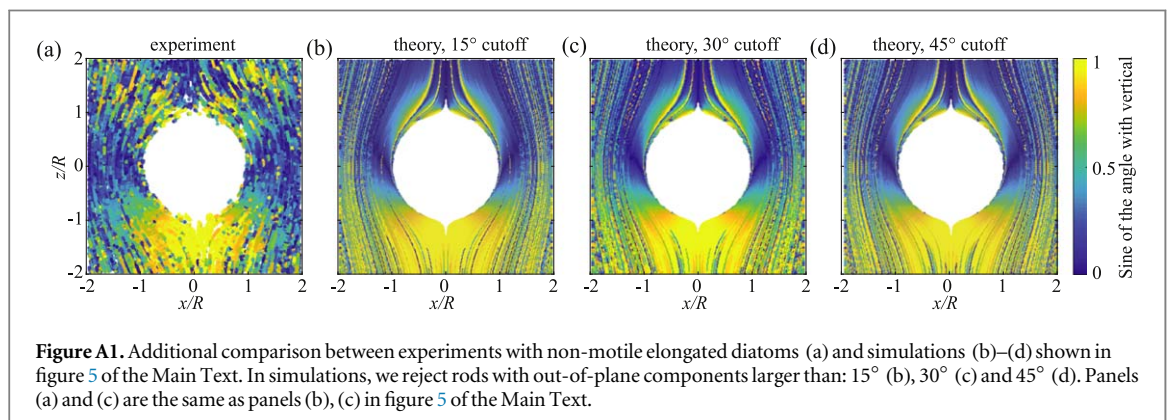
This analysis will also yield the characteristic timescales of the convergence onto the asymptotically stable solutions. As discussed in section 3.1 and in [18], the fixed points of equation (A1) are given by the real eigenvectors of  $\mathbf{A}^T$ . Let  $\boldsymbol{\lambda}$  be a normalized real eigenvector of  $\mathbf{A}^T$  with eigenvalue  $\lambda$ . Linearizing equation (A1) around  $\boldsymbol{\lambda}$  by writing  $\mathbf{p} = \boldsymbol{\lambda} + \Delta\mathbf{p}$ , where the perturbation  $\Delta\mathbf{p}$  lies in the tangent space to the sphere at  $\boldsymbol{\lambda}$ , gives

$$\dot{\Delta\mathbf{p}} = -\lambda\Delta\mathbf{p} + (\mathbf{I} - \boldsymbol{\lambda}\boldsymbol{\lambda}^T)(\mathbf{A}^T\Delta\mathbf{p}). \quad (\text{A2})$$

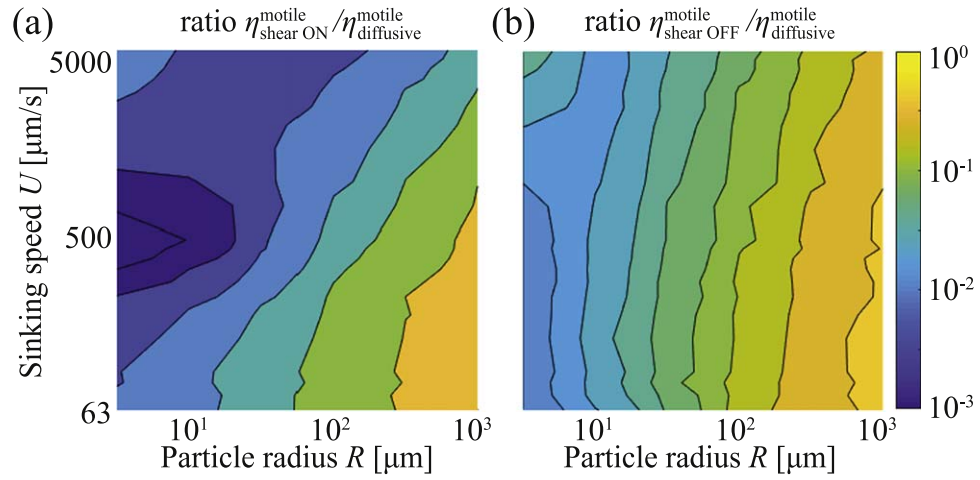
Equation (A2) is a two-dimensional linear dynamical system whose stability can be classified using the standard trace-determinant characterization. To be more explicit, we introduce the basis vectors  $\{\mathbf{e}_1, \mathbf{e}_2\}$  for the tangent space to the sphere at  $\boldsymbol{\lambda}$

$$\mathbf{e}_1 = \mathbf{n} \times \boldsymbol{\lambda}, \quad \mathbf{e}_2 = \mathbf{e}_1 \times \boldsymbol{\lambda}, \quad (\text{A3})$$

where  $\mathbf{n}$  is an arbitrary non-zero vector, non-collinear with  $\boldsymbol{\lambda}$ . In that basis, the perturbation reads  $\Delta\mathbf{p} = \alpha(t)\mathbf{e}_1 + \beta(t)\mathbf{e}_2$  and the linearized system (A2) reduces to







**Figure A2.** Ratios of the encounter efficiencies with and without the impact of shear,  $\eta_{\text{shear ON}}^{\text{motile}}$  (a) and  $\eta_{\text{shear OFF}}^{\text{motile}}$  (b), and the encounter efficiency based on the classical diffusive calculation  $\eta_{\text{diffusive}}^{\text{motile}}$ ; all parameters are the same as in figures 9 and 10 of the Main Text.

In the presence of flow, the diffusive encounter efficiency is given by  $\eta_{\text{diffusive}}^{\text{motile}} = 4Sh/Pe$ , where  $Sh$  and  $Pe$  are the Sherwood and Péclet number, respectively [25]. For the Sherwood number, we used the following formula valid for low Reynolds number  $Sh = 0.5[1 + (1 + 2Pe)^{1/3}]$ . For the Péclet number, we took  $Pe = UR/D_b$ , with the bacterial diffusivity  $D_b = 0.5U_b^2\tau_d$ , where  $\tau_d = D_T^{-1}$ ; for the parameters used,  $D_b = 5 \times 10^{-5}\text{cm}^2\text{ s}^{-1}$ . As discussed in section 6, the diffusive encounter efficiency overestimates the ballistic one and only for the largest sinking particles considered here the two descriptions start to become comparable.

$$\begin{bmatrix} \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = -\lambda \begin{bmatrix} \alpha \\ \beta \end{bmatrix} + \begin{bmatrix} \mathbf{e}_1^T A^\gamma \mathbf{e}_1 & \mathbf{e}_1^T A^\gamma \mathbf{e}_2 \\ \mathbf{e}_2^T A^\gamma \mathbf{e}_1 & \mathbf{e}_2^T A^\gamma \mathbf{e}_2 \end{bmatrix} \begin{bmatrix} \alpha \\ \beta \end{bmatrix} = M_\lambda \begin{bmatrix} \alpha \\ \beta \end{bmatrix}, \quad (\text{A4})$$

where

$$M_\lambda = \begin{bmatrix} \mathbf{e}_1^T A^\gamma \mathbf{e}_1 - \lambda & \mathbf{e}_1^T A^\gamma \mathbf{e}_2 \\ \mathbf{e}_2^T A^\gamma \mathbf{e}_1 & \mathbf{e}_2^T A^\gamma \mathbf{e}_2 - \lambda \end{bmatrix}. \quad (\text{A5})$$

To evaluate the trace and determinant of  $M_\lambda$ , we first note that  $\{\mathbf{e}_1, \mathbf{e}_2, \boldsymbol{\lambda}\}$  is an orthogonal basis for  $A^\gamma$ . In that basis,  $A^\gamma$  takes the form

$$A^\gamma = \begin{bmatrix} \mathbf{e}_1^T A^\gamma \mathbf{e}_1 & \mathbf{e}_1^T A^\gamma \mathbf{e}_2 & 0 \\ \mathbf{e}_2^T A^\gamma \mathbf{e}_1 & \mathbf{e}_2^T A^\gamma \mathbf{e}_2 & 0 \\ \boldsymbol{\lambda}^T A^\gamma \mathbf{e}_1 & \boldsymbol{\lambda}^T A^\gamma \mathbf{e}_2 & \lambda \end{bmatrix}. \quad (\text{A6})$$

Let  $\{\lambda_a, \lambda_b, \lambda\}$  be the three eigenvalues of  $A^\gamma$ . The following identities follow from the above matrix representation

$$\text{Tr} A^\gamma = \mathbf{e}_1^T A^\gamma \mathbf{e}_1 + \mathbf{e}_2^T A^\gamma \mathbf{e}_2 + \lambda = \lambda_a + \lambda_b + \lambda = 0, \quad (\text{A7})$$

$$\det A^\gamma = \lambda_a \lambda_b \lambda = \lambda [(\mathbf{e}_1^T A^\gamma \mathbf{e}_1)(\mathbf{e}_2^T A^\gamma \mathbf{e}_2) - (\mathbf{e}_1^T A^\gamma \mathbf{e}_2)(\mathbf{e}_2^T A^\gamma \mathbf{e}_1)], \quad (\text{A8})$$

where we used fluid incompressibility in the first equation. From the above, we derive the following formulae

$$\mathbf{e}_1^T A^\gamma \mathbf{e}_1 + \mathbf{e}_2^T A^\gamma \mathbf{e}_2 = -\lambda, \quad (\text{A9})$$

$$(\mathbf{e}_1^T A^\gamma \mathbf{e}_1)(\mathbf{e}_2^T A^\gamma \mathbf{e}_2) - (\mathbf{e}_1^T A^\gamma \mathbf{e}_2)(\mathbf{e}_2^T A^\gamma \mathbf{e}_1) = \lambda_a \lambda_b, \quad (\text{A10})$$

which imply the following expressions for the trace and determinant of  $M$

$$\text{Tr} M_\lambda = -3\lambda, \quad (\text{A11a})$$

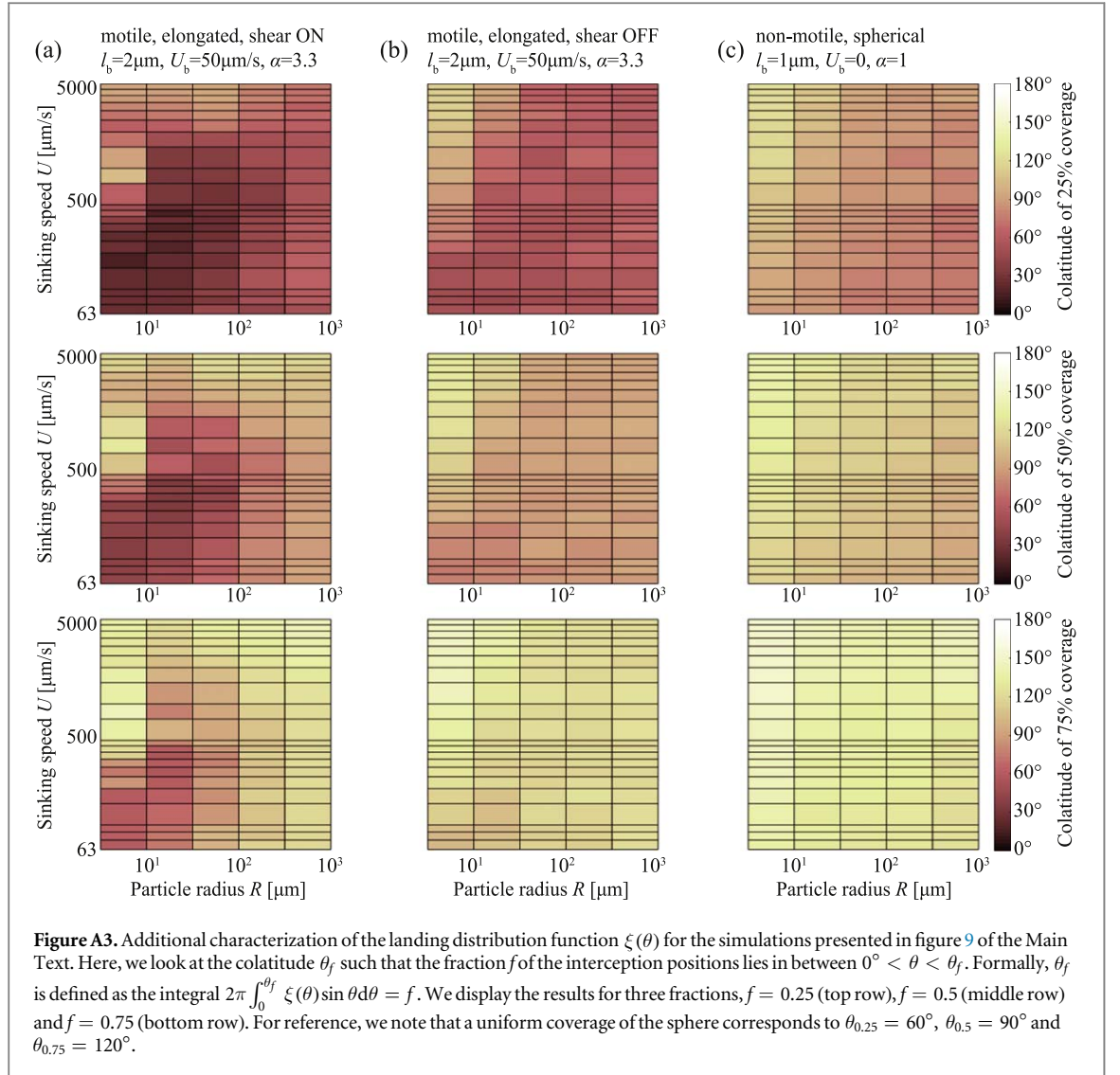
$$\det M_\lambda = 2\lambda^2 + \lambda_a \lambda_b. \quad (\text{A11b})$$

From these expression, the eigenvalues of  $M_\lambda$  read

$$\lambda_\pm^{M_\lambda} = \frac{1}{2}(\text{Tr} M_\lambda \pm \sqrt{\text{Tr} M_\lambda^2 - 4 \det M_\lambda}) = \frac{1}{2}(-3\lambda \pm \sqrt{\lambda^2 - 4\lambda_a \lambda_b}). \quad (\text{A12})$$

Since  $\lambda = -\lambda_a - \lambda_b$  this further simplifies to

$$\lambda_\pm^{M_\lambda} = \frac{1}{2}(-3\lambda \pm \sqrt{(\lambda_a - \lambda_b)^2}). \quad (\text{A13})$$



We now use the eigenvalues (A13) to analyze the linear stability of the fixed points of the Jeffery equation (A1). Let us first consider the case when  $A^7$  has all real eigenvalues  $\lambda_1 < \lambda_2 < \lambda_3$  with eigenvectors  $\{\lambda_1, \lambda_2, \lambda_3\}$ , which are also the fixed points of equation (A1). In this case, the eigenvalues of the linearized system (A4) are also real and equation (A13) simplifies to

$$\lambda_{\pm}^{M_{\lambda}} = \frac{1}{2}(-3\lambda \pm |\lambda_a - \lambda_b|). \quad (\text{A14})$$

Furthermore, since  $\lambda_1 + \lambda_2 + \lambda_3 = 0$  by the incompressibility, we must have  $\lambda_1 = -|\lambda_1| < 0$ ,  $\lambda_3 > 0$  and  $|\lambda_2| < \min(|\lambda_1|, \lambda_3)$ . For the fixed point  $\lambda_1$ , the eigenvalues are always positive

$$\lambda_{\pm}^{M_{\lambda_1}} = \frac{1}{2}(-3\lambda_1 \pm |\lambda_3 - \lambda_2|) = \frac{1}{2}[-3\lambda_1 \pm (\lambda_3 - \lambda_2)] = \frac{1}{2}[-3\lambda_1 \pm (-\lambda_1 - 2\lambda_2)] > 0, \quad (\text{A15})$$

implying that  $\lambda_1$  is a repulsive node. For the fixed point  $\lambda_2$ , the eigenvalues are

$$\lambda_{\pm}^{M_{\lambda_2}} = \frac{1}{2}(-3\lambda_2 \pm |\lambda_1 - \lambda_3|) = \frac{1}{2}(-3\lambda_2 \pm |\lambda_2 + 2\lambda_3|) = \frac{1}{2}[-3\lambda_2 \pm (\lambda_2 + 2\lambda_3)]. \quad (\text{A16})$$

Explicitly

$$\lambda_+^{M_{\lambda_2}} = \lambda_3 - \lambda_2 > 0, \quad (\text{A17a})$$

$$\lambda_-^{M_{\lambda_2}} = -2\lambda_2 - \lambda_3 = \lambda_1 - \lambda_2 < 0. \quad (\text{A17b})$$

Thus,  $\lambda_2$  is a saddle point. Finally, for  $\lambda_3$ , the eigenvalues are always negative

$$\lambda_{\pm}^{M_{\lambda_3}} = \frac{1}{2}(-3\lambda_3 \pm |\lambda_1 - \lambda_2|) = \frac{1}{2}[-3\lambda_3 \pm (\lambda_3 + 2\lambda_2)] < 0, \quad (\text{A18})$$

implying that  $\lambda_3$  is an attracting node. We conclude that the asymptotically stable orientations of equation (A1) for the case when  $A^\gamma$  has three real eigenvalues are given by  $\pm \lambda_3$ , since these are the only attracting fixed points on the sphere of orientations. We can estimate the characteristic time  $\tau_{\lambda_3}$  needed to converge onto the stable orientation  $\lambda_3$  as the inverse of the average of the eigenvalues  $\lambda_{\pm}^{M_{\lambda_3}}$

$$\tau_{\lambda_3}^{-1} = -(\lambda_+^{M_{\lambda_3}} + \lambda_-^{M_{\lambda_3}})/2 = \frac{3}{2}\lambda_3. \tag{A19}$$

We now consider the case when  $A^\gamma$  has a pair of complex conjugate eigenvalues and one real eigenvalue  $\{\lambda_1, \lambda_1^*, \lambda_3\}$ . We write the complex eigenvalue as  $\lambda_1 = \lambda_1^r + i\lambda_1^i$ . In this case, the only fixed point of the Jeffery equation (A1) is given by the real eigenvector  $\lambda_3$ . We estimate the linear stability of this fixed point. The eigenvalues of the linearized system (A4) become

$$\lambda_{\pm}^{M_{\lambda_3}} = \frac{1}{2}[-3\lambda_3 \pm \sqrt{(\lambda_1 - \lambda_1^*)^2}] = -\frac{3}{2}\lambda_3 \pm i|\lambda_1^i|. \tag{A20}$$

We see that, if the only real eigenvalue  $\lambda_3$  is positive, then  $\lambda_3$  is an attractive spiral. Otherwise, it is a repulsive spiral and the asymptotic state of equation (A1) is given by a stable limit cycle, to be discussed in the next section in more detail. The timescale associated with the convergence on or divergence away from  $\lambda_3$  is given by the absolute value of the real part of  $\lambda_{\pm}^{M_{\lambda_3}}$

$$\tau_{\lambda_3}^{-1} = \frac{3}{2}|\lambda_3|. \tag{A21}$$

### A.2. Limit cycle case

In the case when  $A^\gamma$  has complex eigenvalues  $\lambda_{1,2}$  and the real eigenvalue is negative  $\lambda < 0$ , the asymptotic solution to the Jeffery equation (A1) is given by a limit cycle. The limit cycle is the great circle perpendicular to the real eigenvector  $\mathbf{p}^*$  of  $A^\gamma$ . To show this, we introduce the orthonormal basis

$$\mathbf{n}_1 = \mathbf{w} \times \mathbf{p}^* / \|\mathbf{w} \times \mathbf{p}^*\|, \quad \mathbf{n}_2 = \mathbf{n}_1 \times \mathbf{p}^*, \tag{A22}$$

where  $\mathbf{w}$  is a random non-zero vector. Note that the two orthogonal vectors  $\mathbf{n}_1$  and  $\mathbf{n}_2$  span the plane of the great circle perpendicular to the real eigenvector  $\mathbf{p}^*$ . We look for solutions of the form

$$\mathbf{p}(t) = \sin \theta(t) \mathbf{n}_1 + \cos \theta(t) \mathbf{n}_2. \tag{A23}$$

Plugging the above ansatz into the Jeffery equation (A1) yields

$$\dot{\theta} \cos \theta \mathbf{n}_1 - \dot{\theta} \sin \theta \mathbf{n}_2 = [I - (\sin \theta \mathbf{n}_1 + \cos \theta \mathbf{n}_2)(\sin \theta \mathbf{n}_1^T + \cos \theta \mathbf{n}_2^T)](\sin \theta A^\gamma \mathbf{n}_1 + \cos \theta A^\gamma \mathbf{n}_2). \tag{A24}$$

To simplify the above expression, we introduce the following notation for the submatrix of  $A^\gamma$

$$\mathbf{M} = \begin{bmatrix} \mathbf{n}_1^T A^\gamma \mathbf{n}_1 & \mathbf{n}_1^T A^\gamma \mathbf{n}_2 \\ \mathbf{n}_2^T A^\gamma \mathbf{n}_1 & \mathbf{n}_2^T A^\gamma \mathbf{n}_2 \end{bmatrix}, \tag{A25}$$

and project equation (A24) onto  $\mathbf{n}_1$  and  $\mathbf{n}_2$

$$\dot{\theta} \cos \theta(t) = \sin \theta M_{11} + \cos \theta M_{12} - \sin \theta (\sin^2 \theta M_{11} + \sin \theta \cos \theta M_{12} + \cos \theta \sin \theta M_{21} + \cos^2 \theta M_{22}), \tag{A26}$$

$$\dot{\theta} \sin \theta(t) = -\sin \theta M_{21} - \cos \theta M_{22} + \cos \theta (\sin^2 \theta M_{11} + \sin \theta \cos \theta M_{12} + \cos \theta \sin \theta M_{21} + \cos^2 \theta M_{22}). \tag{A27}$$

We combine the two equations into a single one by taking a linear combination with weights  $\cos \theta$  and  $\sin \theta$

$$\dot{\theta} \cos^2 \theta(t) + \dot{\theta} \sin^2 \theta(t) = \dot{\theta} = \cos \theta \sin \theta M_{11} + \cos^2 \theta M_{12} - \sin^2 \theta M_{21} - \sin \theta \cos \theta M_{22}, \tag{A28}$$

which further simplifies to

$$\dot{\theta} = \frac{M_{11} - M_{22}}{2} \sin 2\theta + \frac{M_{12} + M_{21}}{2} \cos 2\theta + \frac{M_{12} - M_{21}}{2}. \tag{A29}$$

Introducing  $A = M_{11} - M_{22}$ ,  $B = M_{12} + M_{21}$  and  $C = M_{12} - M_{21}$ , we obtain

$$2\dot{\theta} = A \sin 2\theta + B \cos 2\theta + C. \tag{A30}$$

This is a first-order nonlinear differential equation. Since the nonlinear term is smooth, the unique (up to the  $2\pi$  period) solution exists, which validates the ansatz (A23) and proves the existence of a limit cycle.

We now explicitly calculate the period  $T$  of the limit cycle. To this end, integrate equation (A30) over  $T$

$$4\pi = CT + \int_0^T (A \sin 2\theta + B \cos 2\theta) dt \tag{A31}$$

$$= CT + \int_0^{2\pi} (A \sin 2\theta + B \cos 2\theta) \frac{1}{\theta} d\theta \quad (\text{A32})$$

$$= CT + 2 \int_0^{2\pi} \left( 1 - \frac{C}{A \sin 2\theta + B \cos 2\theta + C} \right) d\theta. \quad (\text{A33})$$

We get the following equation for  $T$

$$T = \int_0^{2\pi} \frac{2}{A \sin 2\theta + B \cos 2\theta + C} d\theta. \quad (\text{A34})$$

This expression can be expressed as

$$T = 2 \int_0^{2\pi} \frac{1}{A \sin \theta' + B \cos \theta' + C} d\theta' = 2 \int_0^{2\pi} \frac{1}{\sqrt{A^2 + B^2} \sin \hat{\theta} + C} d\hat{\theta}, \quad (\text{A35})$$

where we changed variables twice using  $\theta' = 2\theta$  and  $\hat{\theta} = \theta' + \alpha$ , where  $\sin \alpha = B/\sqrt{A^2 + B^2}$  and we used the periodicity of the integrand to keep the integration limit as  $[0, 2\pi)$ . The final integral can be evaluated using contour integration. We first change the variables  $z = \sqrt{A^2 + B^2} e^{i\theta}$ , which yields

$$T = 4 \oint \frac{dz}{z^2 + 2iCz - (A^2 + B^2)}. \quad (\text{A36})$$

We note that  $C^2 > A^2 + B^2$  corresponds to  $A$  having complex eigenvalues, which is the case of interest. In this case, the integrand has one simple pole inside the integration contour (circle of radius  $\sqrt{A^2 + B^2}$  centered at the origin) given by one of the roots of the integrand denominator. Applying the residue theorem, yields

$$T = \frac{4\pi}{\sqrt{C^2 - A^2 - B^2}}. \quad (\text{A37})$$

This can be related to the original matrix  $A$  and its negative real eigenvalue  $\lambda$  as

$$T = \frac{4\pi}{\sqrt{2 \det A / \lambda + \lambda^2 - \text{tr}(A^2)}}. \quad (\text{A38})$$

Assuming the complex eigenvalues take the form  $\lambda_{1,2} = \alpha \pm i\beta$ , this further simplifies to

$$T = \frac{2\pi}{\beta}. \quad (\text{A39})$$

Therefore, the angular frequency of the limit cycle is given by the imaginary part of the complex eigenvalue. These results agree with the analysis in [19] obtained using a different method.

### A.3. Velocity gradient of the Stokes flow around a sphere

In this section, we compute the velocity gradient in equation (13) due to the Stokes flow around a sinking particle. We first carry out the calculation in the curvilinear orthogonal coordinate basis  $\{\partial_r, \partial_\theta, \partial_\phi\}$  with the metric tensor  $g_{ij} = \text{diag}(1, r^2, r^2 \sin^2 \theta)$  and then transform to the usual orthonormal system  $\{\hat{r}, \hat{\theta}, \hat{\phi}\}$ . The transformation between the two systems is encoded in the Jacobian

$$J = \text{diag}(1, r, r \sin \theta). \quad (\text{A40})$$

In the curvilinear system  $\{\partial_r, \partial_\theta, \partial_\phi\}$ , the Stokes flow (2) reads

$$v = v^r \partial_r + v^\theta \partial_\theta = U \cos \theta \left( 1 + \frac{R^3}{2r^3} - \frac{3R}{2r} \right) \partial_r + U \sin \theta \left( -\frac{1}{r} + \frac{R^3}{4r^4} + \frac{3R}{4r^2} \right) \partial_\theta. \quad (\text{A41})$$

To compute the velocity gradient (1, 1)-tensor  $A_{ij} = \nabla_j v^i$ , we note that the only non-zero Christoffel symbols are

$$\Gamma_{\theta\theta}^r = -r, \quad \Gamma_{\phi\phi}^r = -r \sin^2 \theta, \quad (\text{A42})$$

$$\Gamma_{r\theta}^\theta = \Gamma_{\theta r}^\theta = 1/r, \quad \Gamma_{\phi\phi}^\theta = -\sin \theta \cos \theta, \quad (\text{A43})$$

$$\Gamma_{r\phi}^\phi = \Gamma_{\phi r}^\phi = 1/r, \quad \Gamma_{\theta\phi}^\phi = \Gamma_{\phi\theta}^\phi = \cot \theta. \quad (\text{A44})$$

Using covariant differentiation, we find the velocity gradient tensor components (in the  $\{\partial_r, \partial_\theta, \partial_\phi\}$  basis)

$$\nabla_r v^r = \partial_r v^r, \quad \nabla_r v^\theta = \partial_r v^\theta + v^\theta/r, \quad \nabla_r v^\phi = 0, \quad (\text{A45a})$$

$$\nabla_\theta v^r = \partial_\theta v^r - r v^\theta, \quad \nabla_\theta v^\theta = \partial_\theta v^\theta + v^r/r, \quad \nabla_\theta v^\phi = 0, \quad (\text{A45b})$$

$$\nabla_\phi v^r = 0, \quad \nabla_\phi v^\theta = 0, \quad \nabla_\phi v^\phi = v^r/r + \cot \theta v^\theta. \quad (\text{A45c})$$

Explicit calculation gives the following expressions for the tensor entries

$$\nabla_r v^r = U \cos \theta \left( -\frac{3R^3}{2r^4} + \frac{3R}{2r^2} \right), \quad (\text{A46a})$$

$$\nabla_r v^\theta = U \sin \theta \left( \frac{1}{r^2} - \frac{R^3}{r^5} - \frac{3R}{2r^3} \right) + U \sin \theta \left( -\frac{1}{r^2} + \frac{R^3}{4r^5} + \frac{3R}{4r^3} \right) = U \sin \theta \left( -\frac{3R^3}{4r^5} - \frac{3R}{4r^3} \right), \quad (\text{A46b})$$

$$\nabla_r v^\phi = 0, \quad (\text{A46c})$$

$$\nabla_\theta v^r = -U \sin \theta \left( 1 + \frac{R^3}{2r^3} - \frac{3R}{2r} \right) + U \sin \theta \left( 1 - \frac{R^3}{4r^3} - \frac{3R}{4r} \right) = U \sin \theta \left( -\frac{3R^3}{4r^3} + \frac{3R}{4r} \right), \quad (\text{A46d})$$

$$\nabla_\theta v^\theta = U \cos \theta \left( -\frac{1}{r} + \frac{R^3}{4r^4} + \frac{3R}{4r^2} \right) + U \cos \theta \left( \frac{1}{r} + \frac{R^3}{2r^4} - \frac{3R}{2r^2} \right) = U \cos \theta \left( \frac{3R^3}{4r^4} - \frac{3R}{4r^2} \right), \quad (\text{A46e})$$

$$\nabla_\theta v^\phi = 0, \quad (\text{A46f})$$

$$\nabla_\phi v^r = 0, \quad (\text{A46g})$$

$$\nabla_\phi v^\theta = 0, \quad (\text{A46h})$$

$$\nabla_\phi v^\phi = U \cos \theta \left( \frac{1}{r} + \frac{R^3}{2r^4} - \frac{3R}{2r^2} \right) + U \cos \theta \left( -\frac{1}{r} + \frac{R^3}{4r^4} + \frac{3R}{4r^2} \right) = U \cos \theta \left( \frac{3R^3}{4r^4} - \frac{3R}{4r^2} \right). \quad (\text{A46i})$$

As a sanity check, we compute the flow divergence

$$\nabla_r v^r + \nabla_\theta v^\theta + \nabla_\phi v^\phi = 0, \quad (\text{A47})$$

which vanishes, as expected. In the matrix form, the above tensor reads ( $U = 1$  and  $R = 1$ )

$$A_{ij} = \nabla_j v^i = \begin{bmatrix} \left( -\frac{3}{2r^4} + \frac{3}{2r^2} \right) \cos \theta & \left( -\frac{3}{4r^3} + \frac{3}{4r} \right) \sin \theta & 0 \\ \left( -\frac{3}{4r^5} - \frac{3}{4r^3} \right) \sin \theta & \left( \frac{3}{4r^4} - \frac{3}{4r^2} \right) \cos \theta & 0 \\ 0 & 0 & \left( \frac{3}{4r^4} - \frac{3}{4r^2} \right) \cos \theta \end{bmatrix}. \quad (\text{A48})$$

Finally, we use the Jacobian  $J$  (equation (A40)) to express  $A$  in the orthonormal basis  $\{\hat{r}, \hat{\theta}, \hat{\phi}\}$

$$JAJ^{-1} = \frac{3}{4} \left( \frac{1}{r^2} - \frac{1}{r^4} \right) \cos \theta \begin{bmatrix} 2 & \tan \theta & 0 \\ -\frac{r^2+1}{r^2-1} \tan \theta & -1 & 0 \\ 0 & 0 & -1 \end{bmatrix}, \quad (\text{A49})$$

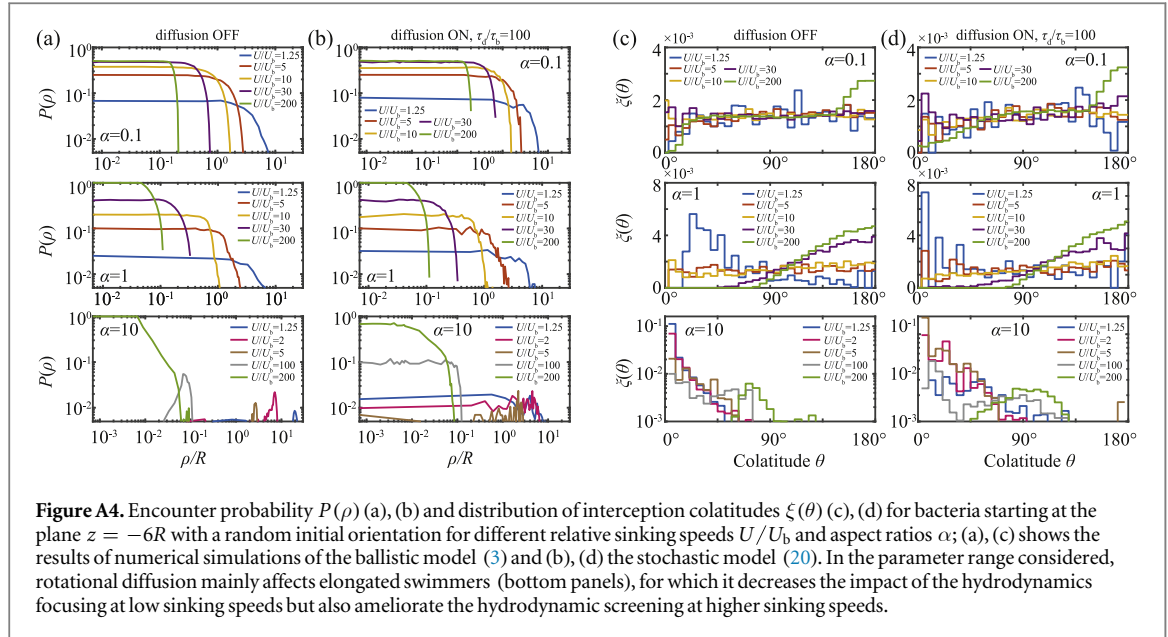
which yields equation (13), in agreement with the calculation in [21] where the velocity gradient was computed using a different method.

#### A.4. Ellipsoids in the Stokes flow: stagnation lines and particle surface

The eigenvalues of the velocity gradient  $A$  (equation (13)) on the stagnation line ( $\theta = 0, \pi$ ) and the particle surface ( $r = 1$ ) have multiplicity greater than one. In this case, the analysis of section 3.1 does not directly apply, yet these special locations will be important for the encounter process of non-motile micro-organisms, which can only approach the sinking particle near the stagnation line  $\theta = \pi$ . On the stagnation lines  $\theta = 0, \pi$ , equation (13) reduces to

$$A_{ij}(r, \theta = 0, \pi, \phi) = \pm \frac{3}{4} \left( \frac{1}{r^2} - \frac{1}{r^4} \right) \begin{bmatrix} 2 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{bmatrix}, \quad (\text{A50})$$

where  $\pm$  corresponds to  $\theta = 0$  and  $\theta = \pi$ , respectively. This simple diagonal structure implies that on the upstream stagnation line ( $\theta = \pi$ ) rods align tangentially to the sinking particle, while on the downstream stagnation line ( $\theta = 0$ ), rods align vertically. This picture can be inferred from figure 3(b) by taking the limit  $\rho \rightarrow 0$ . Since  $A^{\gamma=-1} = -A^T$ , we immediately obtain the response of disks. Disks align tangentially to the particle surface for  $\theta = \pi$  (with axis of symmetry in the vertical direction), while they lie in the  $r - \theta$  plane for  $\theta = 0$ . Therefore, non-motile rods or disks approaching the sinking particle along the  $\theta = \pi$  stagnation line orient with their longer dimension tangential to the particle surface. We now compute  $A$  on the particle surface to see if shear tends to maintain such a tangential orientation. At  $r = 1$ , the only non-zero component of the velocity gradient is  $A_{\theta r}(r = 1, \theta, \phi) = -\frac{3}{2} \sin \theta$ . This structure implies that the tangential orientations of rods (symmetry axis along  $\theta - \phi$ ) and disks (symmetry axis along  $r$ ) are the null vectors. Thus, to zeroth order, shear maintains the tangential orientation of rods and disks as they are advected around the sinking particle.



## A.5. Methods: numerical simulations

**A.5.1. Time stepping.** To numerically integrate the ballistic model (equation (3)), we discretized the equations of motion using the classical Runge–Kutta method (RK4). Depending on the sinking speed, the time-step was chosen between  $\Delta t = 0.075\tau_b$  for  $U \sim U_b$  and  $\Delta t = 0.005\tau_b$  for  $U \sim 100U_b$ , where  $\tau_b = l_b/U_b$  is the time needed for the bacterium to travel distance equal to its bodylength. To integrate the quasi-ballistic model with rotational diffusion (equation (20)), we used the stochastic version of the Euler method; at each time step, the diffusive term is discretized by sampling a  $3 \times 1$  vector with normally distributed entries with zero mean and variance  $2D_r \Delta t$ . With the rotational diffusion coefficient  $D_r = 0.25 \text{ s}^{-1}$ , the time step varied between 0.04 and 0.2 ms. At each time step, the bacterial orientational vector was normalized to unit length.

**A.5.2. Estimation of the encounter efficiency.** For a given sinking particle size  $R$  and sinking speed  $U$ , we estimated the encounter efficiency by discretizing equation (7). We typically sampled the encounter probability  $P(\rho)$  on a non-uniform grid to resolve the accumulation of  $P(\rho)$  near the accessibility region for slowly sinking particles or near the centerline for fast sinking particles (see figures 7 and A4); the number of points on the  $\rho$ -grid was always at least 50 for motile bacteria and 10 for non-motile bacteria. Once the estimate of  $P(\rho)$  had been obtained, the integral in equation (7) was evaluated using the trapezoidal rule.

To estimate the encounter probability  $P(\rho)$  starting in the initial plane  $z = -6R$  at distance  $\rho$  away from the centerline for random initial orientations, we considered an ensemble of initial orientations by sampling along a spherical spiral. Such a sampling gives an approximately uniform distribution of points on a unit sphere of orientations. By using spherical spiral to sample initial orientations rather than choosing them randomly (that is, choosing  $3 \times 1$  vectors with normal entries with zero mean and normalizing them to unit length), we obtained faster convergence by avoiding random clustering of points on the unit sphere. The number of initial orientations was chosen high enough to guarantee that the solid angle the sinking particle extended at the initial bacterial location contained at least five initial orientations (the number of blue dots in the inset in figure 1 was always at least five). For such an angular resolution, the number of initial orientations varied between  $O(10^2)$  for fast sinking particles up to  $O(10^4)$  for slowly sinking particles, for which the accessibility region with  $P(\rho) > 0$  was largest. In general, to estimate the encounter efficiency  $\eta$  for a given  $(R, U)$  pair, we simulated about  $O(10^4)$  trajectories for fast sinking particles and up to  $O(10^6)$  trajectories for slowly sinking particles. In total, due to scanning the  $(R, U)$  parameter space in different shear ON/OFF configurations, the this work summarizes the results of simulating about  $O(10^8)$  bacterial trajectories.

**A.5.3. Interception criterion.** The sinking particle was assumed to be a perfect absorber: geometric overlap between any part of a bacterium and the particle was counted as an encounter. In simulations, for simplicity, we computed this geometric overlap by approximating elongated bacteria ( $\alpha > 1$ ) of length  $l_b$  by a cylinder with spherical caps. The cylinder length, including caps, is  $l_b$  and its width is  $l_b/\alpha$ . With this simplification, determining the interception is equivalent to determining the distance between the cylinder centerline and the particle center. Similarly, the geometry of oblate particles ( $\alpha < 1$ ) was approximated by considering four



cylinders (with spherical caps) of length  $l_b$  and width  $l_b \alpha$ . The centerlines of the cylinders lie in a plane, the centerline midpoints coincide and the centerlines are rotated at angle  $45^\circ$ —the four cylinders form two crosses rotated by  $45^\circ$ . With this simplification, determining the interception is equivalent to determining the distance between the four cylinder centerlines and the particle center.

*A.5.4. Estimation of the distribution of interception locations.* To estimate  $\xi(\theta)$  for a given  $(R, U)$  pair, we considered the ensemble of the endpoints of trajectories that resulted in the interception. As described above, this ensemble resulted from scanning the  $\rho$ -range, the initial position at distance  $\rho$  away from the particle centerline in the initial  $z = -6R$ -plane, as well as uniform initial orientations. This ensemble yielded a histogram of the interception colatitudes  $\theta$ . During construction of this histogram, the counts for each scanned position  $\rho$  were further weighted by  $\rho$  and the  $\rho$ -grid spacing, to account for the number of initial positions at distance  $\rho$  being proportional to  $\rho$  (circles of radius  $\rho$ ) as well as the non-uniformity of the  $\rho$ -grid. Such prepared histogram of  $\theta$ -counts (30 bins, bin width  $6^\circ$ ), normalized to a probability density function over a unit sphere, was used as the estimate of  $\xi(\theta)$ .

## A.6. Methods: experiments

*A.6.1. Cell cultured.* *Phaeodactylum tricornutum* cells (strain CCMP2561) were cultured in  $f/2$  medium (Guillard and Ryther 1962) mixed with artificial seawater. Artificial seawater was prepared by dissolving 35 g of artificial sea salt (Instant Ocean, Spectrum Brands) in 1 l double distilled water (DDW), filtered through a  $0.2 \mu\text{m}$  filter and autoclaved. Cultures were propagated in  $18^\circ\text{C}$  in AlgaeTron AG 230 PSI (Photon Systems Instruments) with 14 h/10 h light/dark cycle. For the experiments, cells in the exponential growing phase were used. Cell length and width were  $21.2 \pm 2.4 \mu\text{m}$  ( $n = 14$ ) and  $3.12 \pm 0.57 \mu\text{m}$  ( $n = 14$ ), respectively, as measured by phase microscopy.

*A.6.2. Experimental procedure.* Alginate beads were prepared using a mix of sodium alginate salt from brown algae (1.5% w/v, medium viscosity; Sigma) with 50 mM ethylenediamine tetra acetic acid (EDTA) in DDW. Beads were prepared by dripping the alginate solution from a 1 ml syringe at rate of  $60 \mu\text{l min}^{-1}$  from a height of 20 cm to beaker containing 0.5 M  $\text{CaCl}_2$  in DDW. The  $\text{CaCl}_2$  solution was stirred at 300 rpm, using a magnetic stir-bar. Flow dynamics were studied in microfluidic chip (Sticky-Slide 0.4—IBIDI). For the experiment, single bead was trapped at the center of the channel using a glass cover slide. A syringe pump (Harvard PHD2000) was then used to feed the channels with artificial sea water at the desired flow speed ( $160 \mu\text{m s}^{-1}$ ). Channel was visualized using a Nikon (eclipse TI-2) microscope at magnification of  $4 \times 1.5 \times 10$  ( $60\times$ ) and 20 fps using Orca flash 4.0 (Hamamatsu) camera.

*A.6.3. Image analysis.* Image analysis was performed on 50 consecutive images using ImageJ (Rueden *et al* 2017). In general  $1098 \pm 50$  cells/image were measured. To extract the orientation from each cell, median image intensity was calculated using ‘Stacks/Z Projection’ function and subtract from all images. ‘FFT/Bang pass’ filter was used with small cutoff of 1 pxl and big cutoff of 10 pxl. ‘Minimum’ filter was used with 1 pxl cutoff. Data was transformed to binary using ‘Make binary’ function with default parameters. Finally, ‘Analyze particle’ function (Particle 30–1000 pxl) was used to collect the orientation data.

## A.7. More details on the impact of rotational diffusion.

The uniformizing impact of diffusion is studied in more detail in figure A4, where we consider the interception probability  $P(\rho)$  for a bacterium starting at the plane  $z = -6R$  with random orientation (figures A4(a), (b)) as well as the corresponding distribution of the interception locations  $\xi(\theta)$  (figures A4(c), (d)). We compare side to side the cases without (figures A4(a), (c)) and with diffusion (figures A4(b), (d)) for oblate, spherical and elongated swimmers (top, middle and bottom rows, respectively). The accessibility region (defined as  $P(\rho) > 0$ ) shrinks under diffusion, because the now erratic motion of bacteria takes longer to reach the particle. and therefore, the bacteria must start closer to the particle to be able to catch it. Within the accessibility region, the distribution  $P(\rho)$  for oblate and spherical swimmers is nearly unaffected by diffusion (figures A4(a), (b), top and middle rows) and so is  $\xi(\theta)$  (figures A4(c), (d), top and middle rows). However, for elongated swimmers, diffusion decreases the size of the high probability belt near the edge of the accessibility region but also raises the probability of interception for initial conditions directly below the sinking particle (figures A4(a), (b), bottom row). As a consequence, diffusive elongated swimmers have non-negligible probability of attaching to the front of the sinking particle (figures A4(c), (d), bottom rows).

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